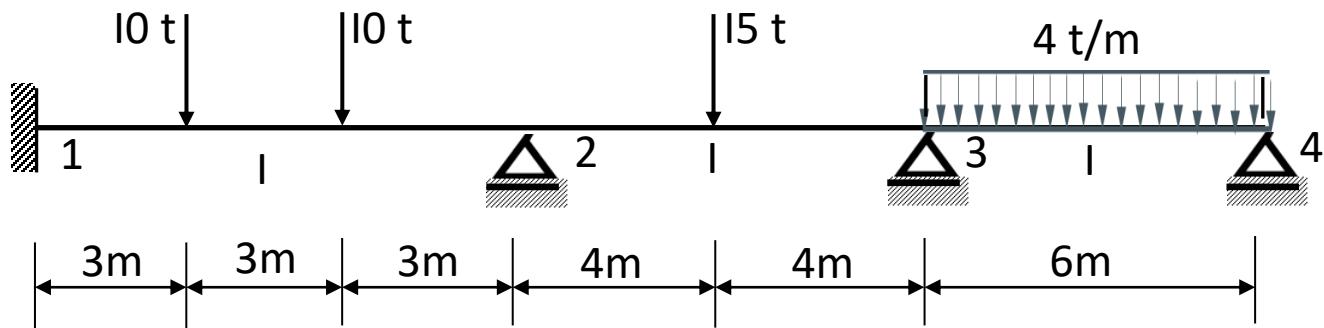


YAPI STATİĞİ 2-HİPERSTATİK SİSTEMLER DEPLASMAN METODLARI(2-4)

Prof. Dr. Cengiz Dündar

ÖRNEK 1

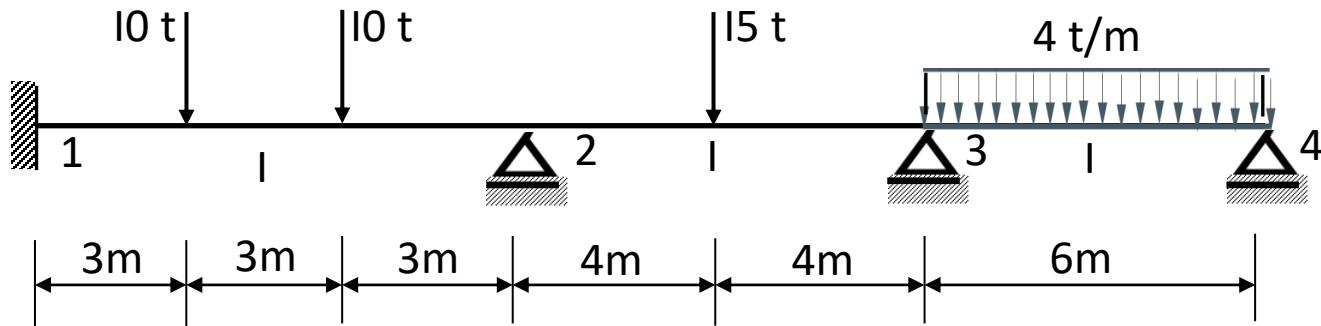


1. Ankastrelik momentleri

$$M_{12} = -M_{21} = \frac{2}{9} PL = \frac{2}{9} * 10 * 9 = 20 \text{ tm}$$

$$M_{23} = -M_{32} = \frac{PL}{8} = \frac{15 * 8}{8} = 15 \text{ tm}$$

$$M_{34} = \frac{qL^2}{8} = \frac{4 * 6^2}{8} = 18 \text{ tm}$$

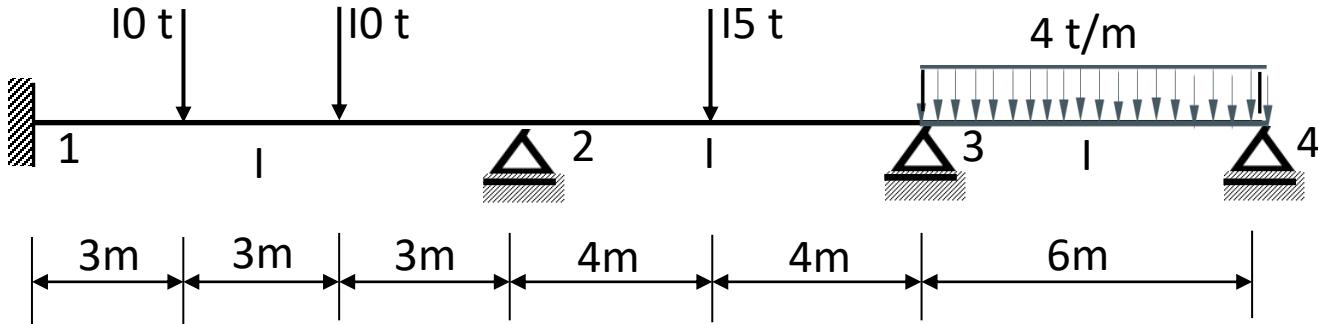


2. Dağıtma sayıları

$$r_{21} = \frac{m_{2\theta_2}^{21}}{m_{2\theta_2}^{21} + m_{2\theta_2}^{23}} = \frac{\frac{4EI}{9}}{\frac{4EI}{9} + \frac{4EI}{8}} = \frac{0.111}{0.111 + 0.125} = 0.47$$

$$r_{23} = \frac{m_{2\theta_2}^{23}}{m_{2\theta_2}^{21} + m_{2\theta_2}^{23}} = \frac{\frac{4EI}{8}}{\frac{4EI}{9} + \frac{4EI}{8}} = \frac{0.125}{0.111 + 0.125} = 0.53$$

$$\sum r = 1 \text{ olmalı} \rightarrow 0.47 + 0.53 = 1 \quad \checkmark$$



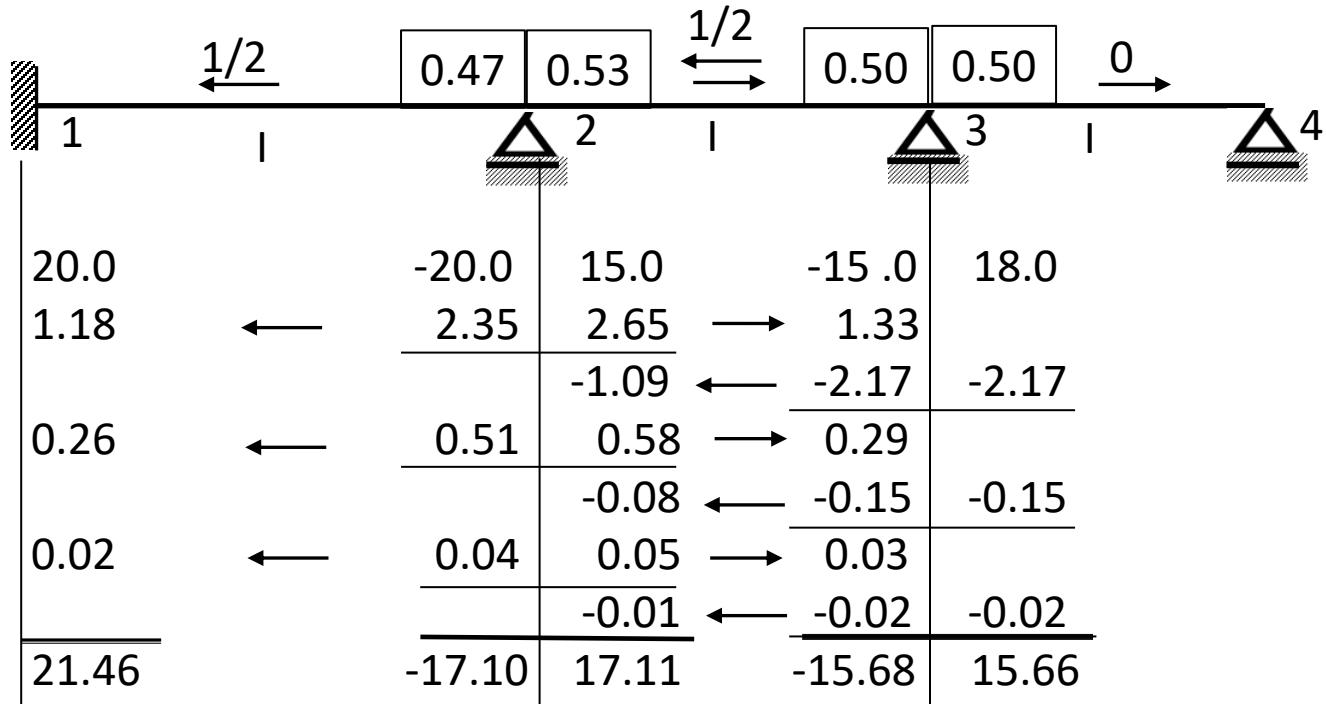
2. Dağıtma sayıları

$$r_{32} = \frac{m_{3\theta_3}^{32}}{m_{3\theta_3}^{32} + m_{3\theta_3}^{34}} = \frac{\frac{4EI}{8}}{\frac{4EI}{8} + \frac{3EI}{6}} = \frac{0.125}{0.125 + 0.125} = 0.50$$

$$r_{34} = \frac{m_{3\theta_3}^{34}}{m_{3\theta_3}^{32} + m_{3\theta_3}^{34}} = \frac{\frac{3EI}{6}}{\frac{4EI}{8} + \frac{3EI}{6}} = \frac{0.125}{0.125 + 0.125} = 0.50$$

$$\sum r = 1 \text{ olmalı} \rightarrow 0.50 + 0.50 = 1 \quad \checkmark$$

3. Dengeleme



Fark momentin büyük olduğu düğümden başlanır

$$2 \text{ düğüm noktasının kilidini çözelim} \quad M_i + M_k = 0 \rightarrow -M_k = M_i \rightarrow M_2 = -20 + 15 = -5 \text{ tm}$$

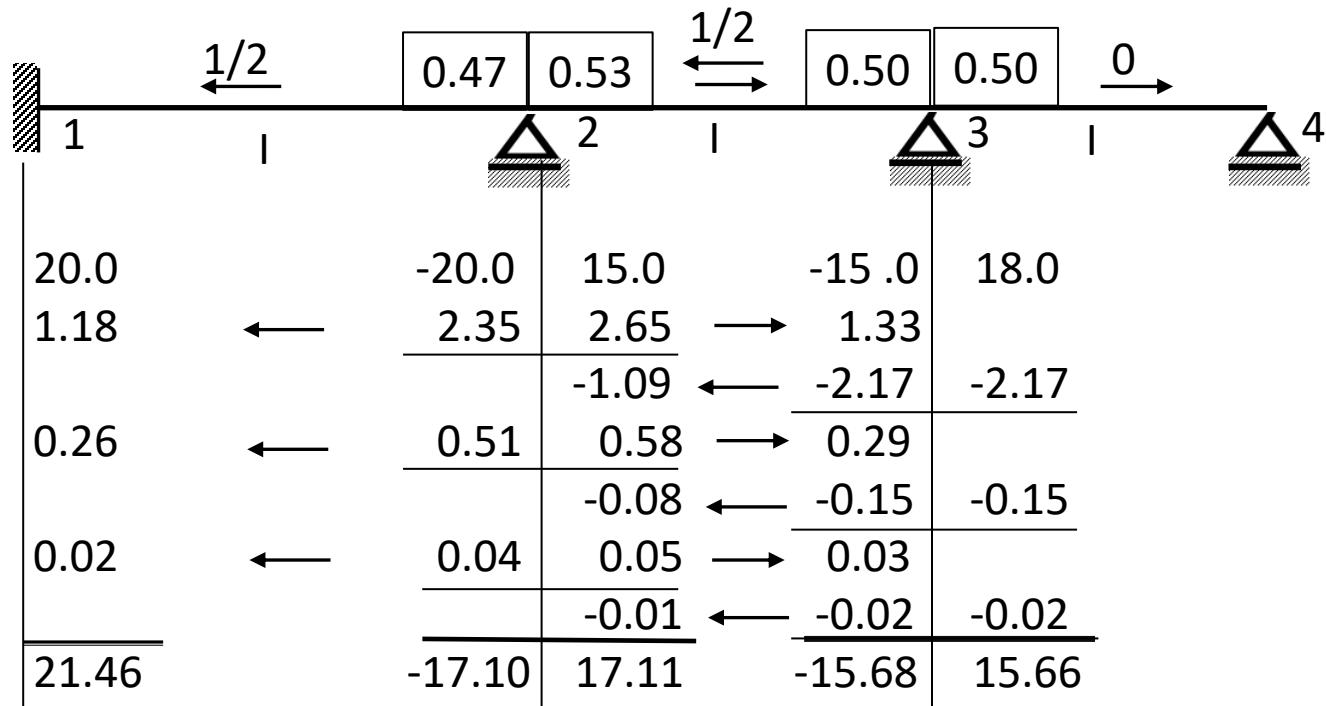
$$-(-5.0) * 0.47 = 2.35 \text{ tm} \quad -(-5.0) * 0.53 = 2.65 \text{ tm}$$

3 düğüm noktasının kilidini çözüp 2 düğüm noktasını kilitleyelim

$$M_i + M_k = 0 \rightarrow -M_k = M_i \rightarrow M_3 = -15 + 18 + 1.33 = 4.33 \text{ tm}$$

$$-(4.33 * 0.50) = -2.17 \text{ tm} \quad -(4.33) * 0.50 = -2.17 \text{ tm}$$

3. Dengeleme

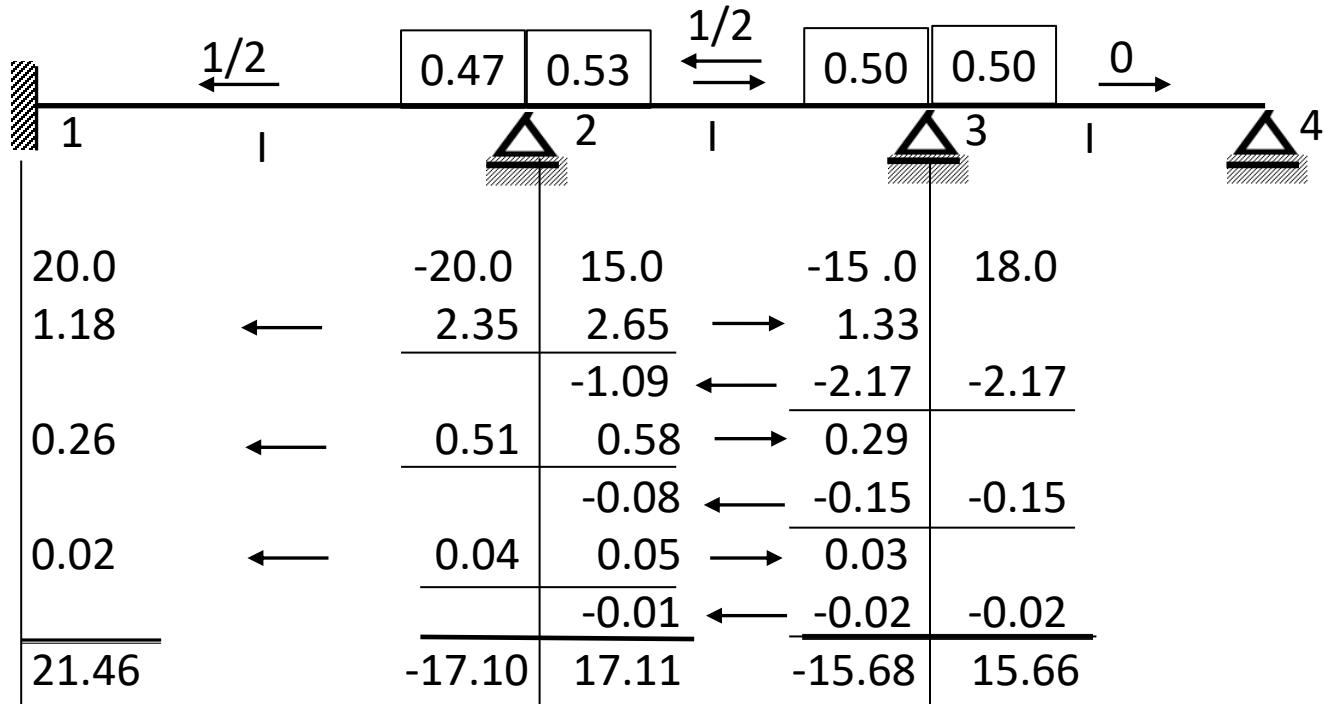


3 düğüm noktasının kilitleyip 2 düğüm noktasının kilidini çözelim

$$M_2 = -1.09 \text{ tm}$$

$$-(-1.09 * 0.47) = 0.51 \text{ tm} \quad -(-1.09) * 0.53 = 0.58 \text{ tm}$$

3. Dengeleme

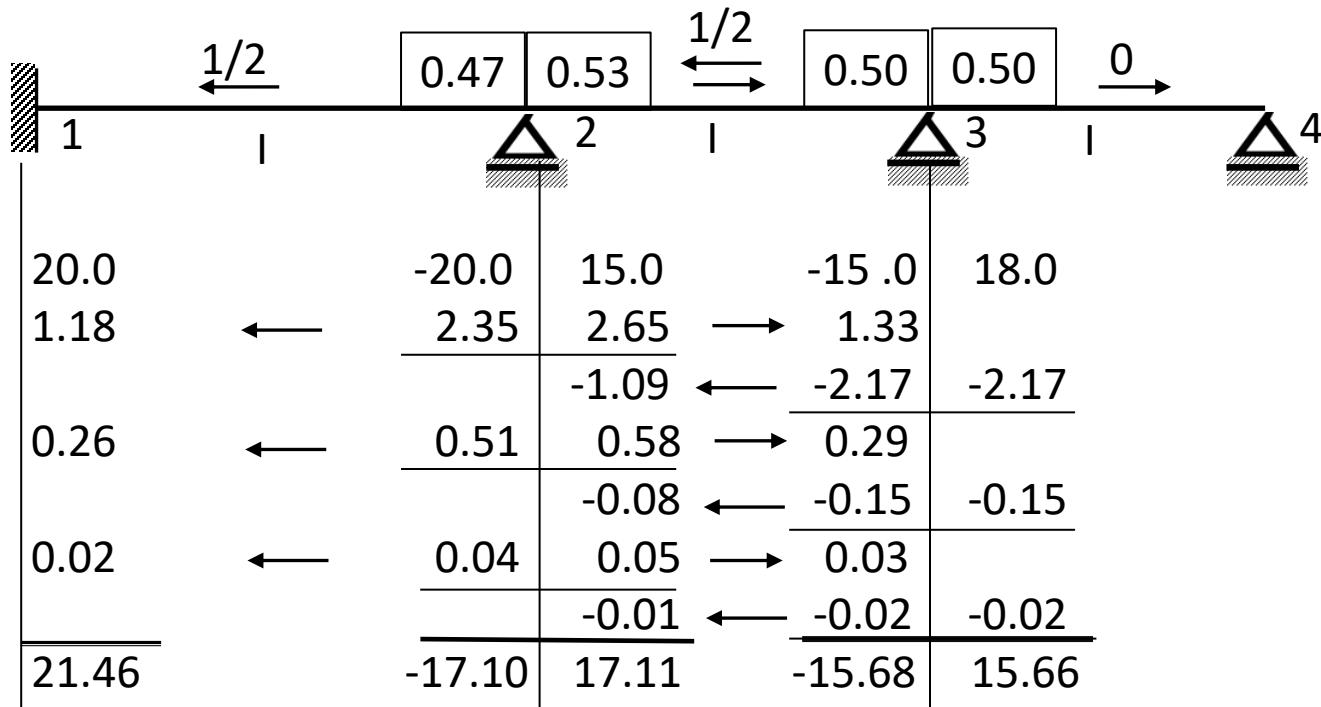


3 düğüm noktasının kilidini çözüp 2 düğüm noktasını kilitleyelim

$$M_3 = 0.29tm$$

$$-(0.29 * 0.50) = -0.15 tm \quad -(0.29) * 0.50 = -0.15 tm$$

3. Dengeleme



4. Süperpozisyon yaparak çubuk uç momentlerinin hesabı

$$M_{12} = 20.0 + 1.18 + 0.26 + 0.02 = 21.46 \text{ tm}$$

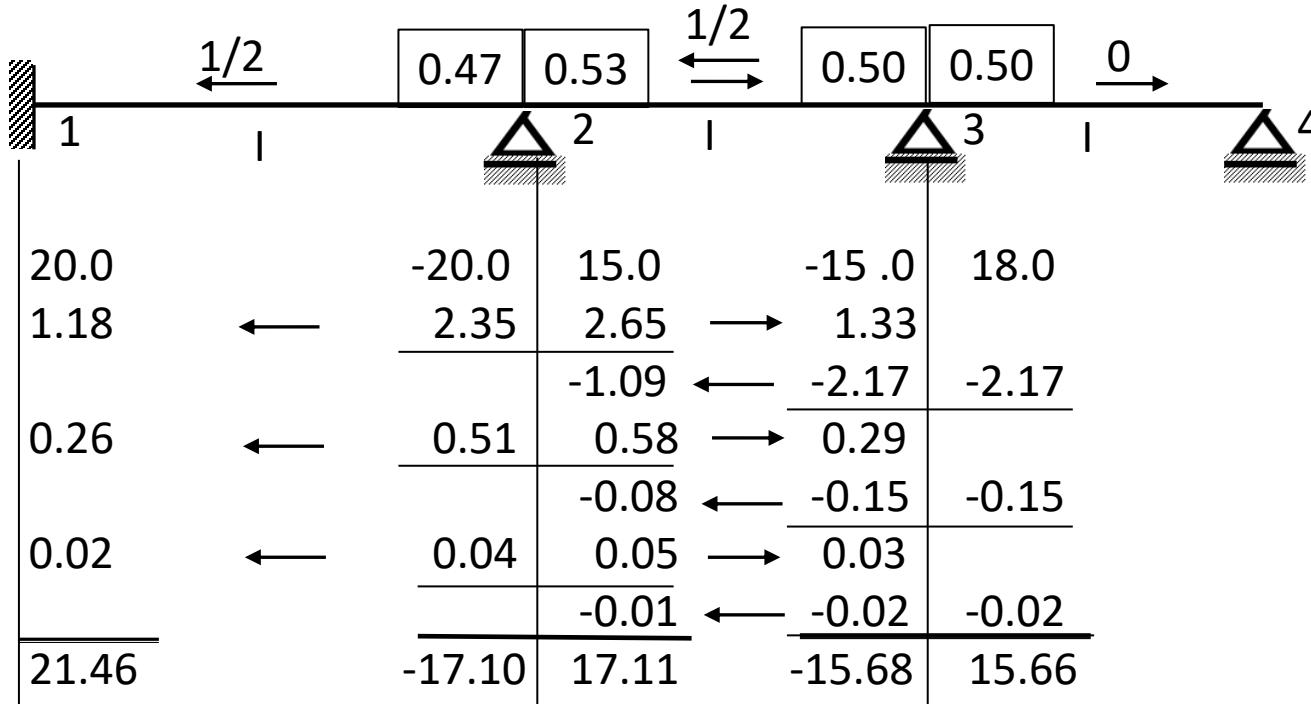
$$M_{21} = -20.0 + 2.35 + 0.51 + 0.04 = -17.10 \text{ tm}$$

$$M_{23} = 15 + 2.65 - 1.09 + 0.58 - 0.08 + 0.05 - 0.01 = 17.11 \text{ tm}$$

$$M_{32} = -15.0 + 1.33 - 2.17 + 0.29 - 0.15 + 0.03 - 0.02 = -15.68 \text{ tm}$$

$$M_{34} = 18.0 - 2.17 - 0.15 - 0.02 = 15.66 \text{ tm}$$

3. Dengeleme

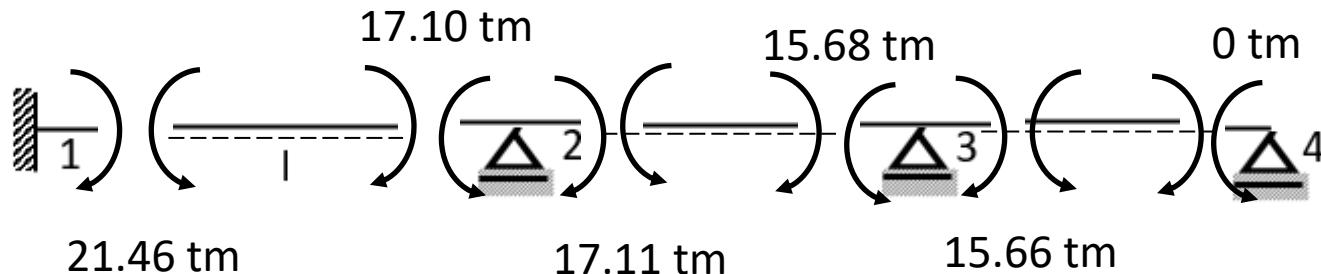


5. 2 ve 3 nolu düğüm noktalarının dönmeleri hesabı

$$\theta_2 = \frac{2.35 + 0.51 + 0.04}{m_{2\theta_2}^{21}} = \frac{2.5}{\frac{4EI}{9}} = \frac{6.52}{EI} rd \quad \theta_2 = \frac{2.65 + 0.58 + 0.05}{m_{2\theta_2}^{23}} = \frac{3.28}{\frac{4EI}{8}} = \frac{6.52}{EI} rd \quad \checkmark$$

$$\theta_3 = \frac{-2.17 - 0.15 - 0.02}{m_{3\theta_3}^{32}} = \frac{-2.34}{\frac{4EI}{8}} = \frac{-4.68}{EI} rd \quad \theta_3 = \frac{-2.17 - 0.15 - 0.02}{m_{3\theta_3}^{34}} = \frac{-2.34}{\frac{3EI}{6}} = \frac{-4.68}{EI} rd$$

4. Dönüştürme



7. Kesme kuvvetleri hesabı

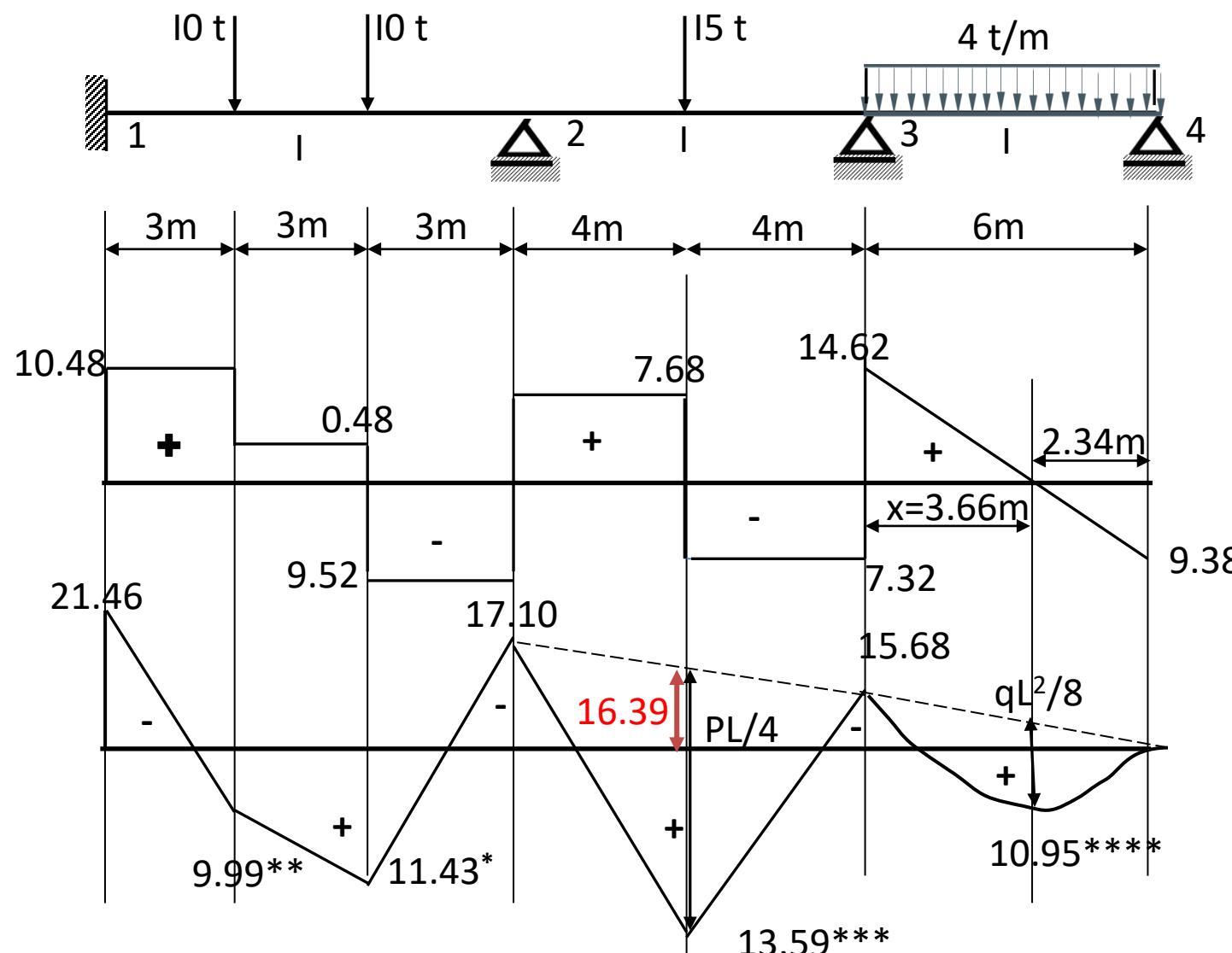
$$T_{1sag} = T_{0ij} + \frac{M_{ij} + M_{ji}}{L} = 10 + \frac{21.46 - 17.10}{9} = 10.48 t \quad T_{2sol} = -10 + \frac{21.46 - 17.10}{9} = -9.52 t$$

$$T_{2sag} = 7.5 + \frac{17.11 - 15.68}{8} = 7.5 + 0.18 = 7.68 t$$

$$T_{3sol} = -7.5 + \frac{17.11 - 15.68}{8} = -7.5 + 0.18 = -7.32 t \quad T_{3sag} = 12 + \frac{15.66}{6} = 14.62 t$$

$$T_{4sol} = -12 + \frac{15.66}{6} = -9.38 t$$

5. Kesme kuvveti ve moment diyagramları



$$*** \frac{17.10 - 15.68}{2} + 15.68 = 16.39$$

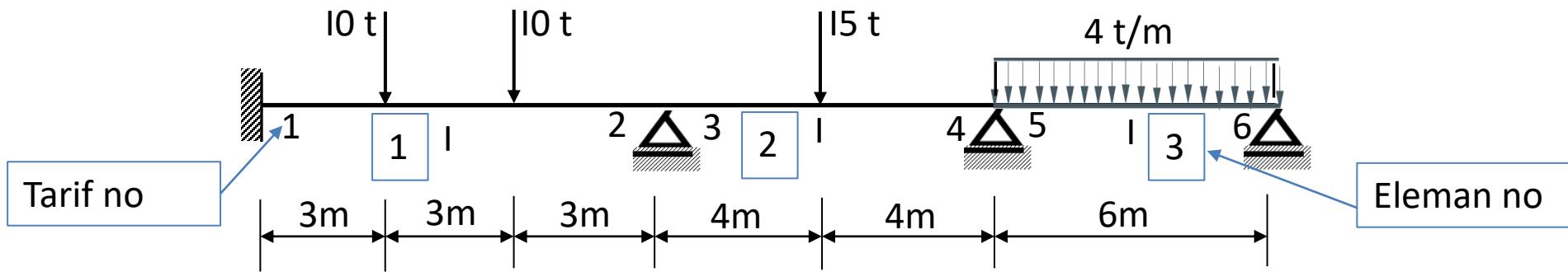
$$*** M_{max} = \frac{15 * 8}{4} - 16.39 = 13.61 \text{ tm}$$

Kesme Kuvveti Diyagramı

$$\frac{14.62}{x} = \frac{9.38}{6-x} \rightarrow x = 3.66 \text{ m}$$

Moment Diyagramı

$$**** M_{max} = \frac{1}{2} * 9.38 * 2.34 = 10.95 \text{ tm}$$



*** C R O S S - Y O N T E M I ***1994

Prof.Dr. Cengiz DUNDAR

Ars.Gor. Bulent SAHIN

3 ACIKLIKLI SUREKLI KIRIS

V E R I D E G E R L E R I:

ELEMAN	BOY	ATALET MOM	DAGITMA KATS
1	9.00	1.000	0.000 0.471
2	8.00	1.000	0.529 0.500
3	6.00	1.000	0.500 1.000

YUKLEME NO= 1

ITERASYON SAYISI=10

ELEMAN	TARIF NO	ANKAS.UC MOM.	BAS.KI.KESME K.
1	1	-20.00	-10.00
	2	20.00	10.00
2	3	-15.00	-7.50
	4	15.00	7.50
3	5	-12.00	-12.00
	6	12.00	12.00

H E S A P L A N A N D E G E R L E R:

*** E L E M A N U C K U V V E T L E R I ***

ELEMAN	TARIF NO	MOMENT	KESME KUVVETI
1	1	-21.449	-10.483
	2	17.102	9.517
2	3	-17.102	-7.677
	4	15.685	7.323
3	5	-15.685	-14.614
	6	0.000	9.386

Xmax(i ucundan)= 3.000

1INCI ELEMAN ACIKLIK MOMENTI= 10.000

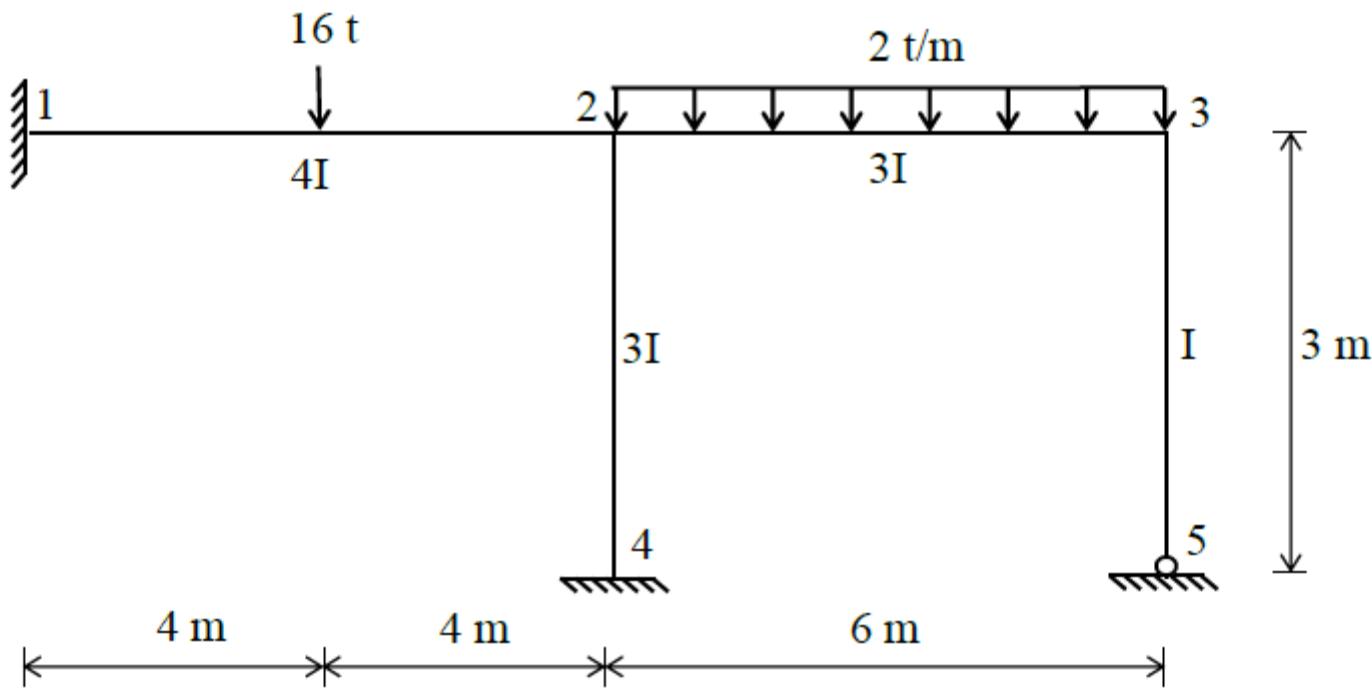
Xmax(i ucundan)= 4.000

2INCI ELEMAN ACIKLIK MOMENTI= 13.606

Xmax(i ucundan)= 3.654

3INCI ELEMAN ACIKLIK MOMENTI= 11.012

ÖRNEK 2



1. Ankastrelilik Momentler

$$-M_{21} = M_{12} = \frac{P l}{8} = \frac{16 \times 8}{8} = 16 \text{ tm}$$

$$M_{23} = -M_{32} = \frac{q l^2}{12} = \frac{2 \times 6^2}{12} = 6 \text{ tm}$$

2. Dağıtma Sayıları

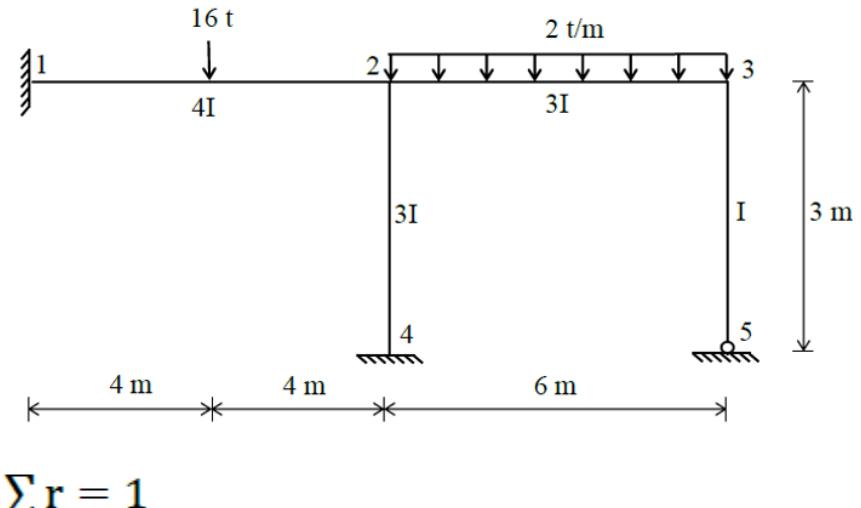
$$r_{21} = \frac{m_{2\theta_2}^{21}}{m_{2\theta_2}^{21} + m_{2\theta_2}^{23} + m_{2\theta_2}^{24}} = \frac{\frac{4E(4I)}{8}}{\frac{4E(4I)}{8} + \frac{4E(3I)}{6} + \frac{4E(3I)}{3}} = 0.25$$

$$r_{23} = \frac{\frac{4E(3I)}{6}}{\frac{4E(4I)}{8} + \frac{4E(3I)}{6} + \frac{4E(3I)}{3}} = 0.25$$

$$r_{24} = \frac{\frac{4E(3I)}{3}}{\frac{4E(4I)}{8} + \frac{4E(3I)}{6} + \frac{4E(3I)}{3}} = 0.50$$

$$r_{32} = \frac{\frac{4E(3I)}{6}}{\frac{4E(3I)}{6} + \frac{3E(I)}{3}} = 0.667$$

$$r_{35} = \frac{\frac{3E(I)}{3}}{\frac{4E(3I)}{6} + \frac{3E(I)}{3}} = 0.333$$



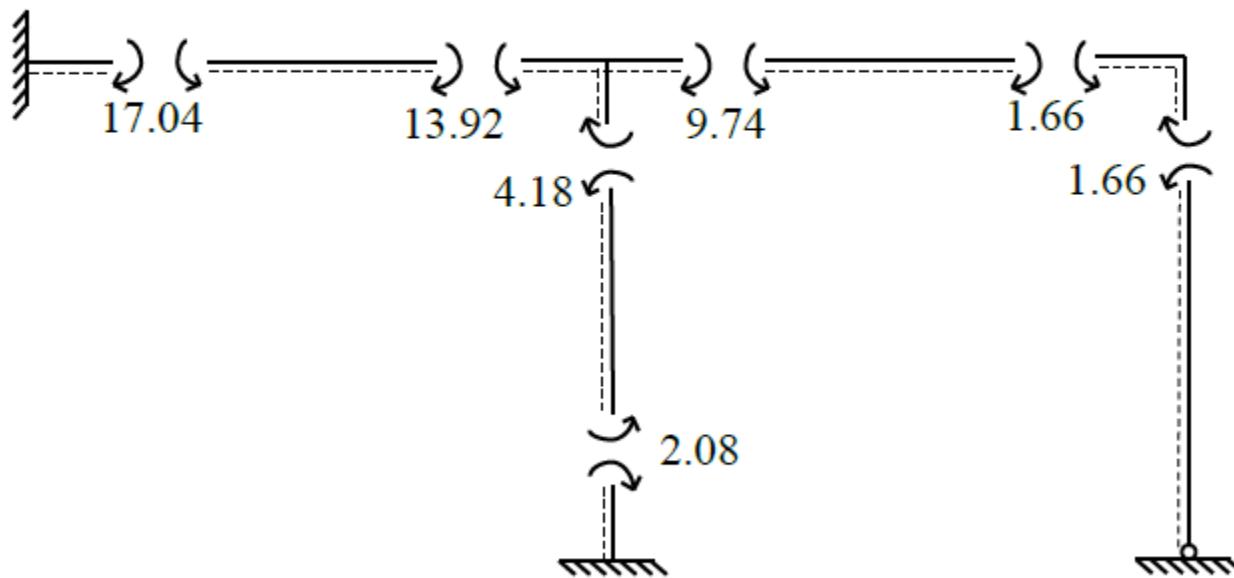
$$\sum r = 1$$

3. Cross Dengelemeleri

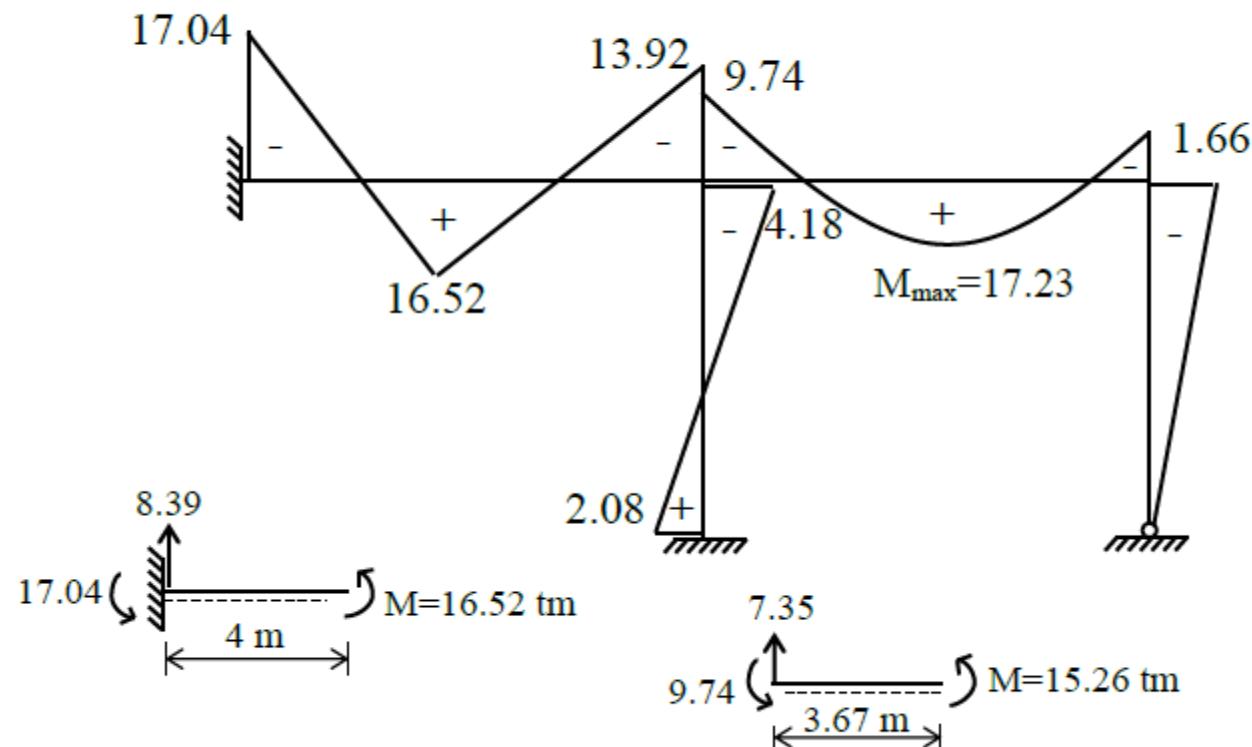
Fark momentin büyük olduğu düğümden başlanır

	$1/2 \leftarrow$	(21) 0.25	(24)	(23) 0.25	\leftrightarrow	1/2 0.667	(32) 0.333	(35)
16.00		-16.00	0 0	6.00		-6.00		
1.25	\leftarrow	2.50	5.00	2.50	\rightarrow	1.25		$-6+1.25=-4.75$
-0.20	\leftarrow	-0.40	-0.79	-0.40	\rightarrow	-0.20	3.17	$-(-4.75) \times 0.667 = 3.17$
<u>-0.01</u>	\leftarrow	<u>-0.02</u>	<u>-0.03</u>	<u>-0.02</u>	\rightarrow	<u>-0.01</u>	<u>0.07</u>	$-(-4.75) \times 0.333 = 1.59$
17.04		-13.92	4.18	9.74		1.66		
			2.50					
			-0.40					
			<u>-0.02</u>					
			2.08					

4. Dönüştürme



5. Moment Diyağramı



6. Uç Kesme Kuvvetlerin Hesabı

$$T_{12} = 8 + \frac{17.04 - 13.92}{8} = 8.39 \text{ t}$$

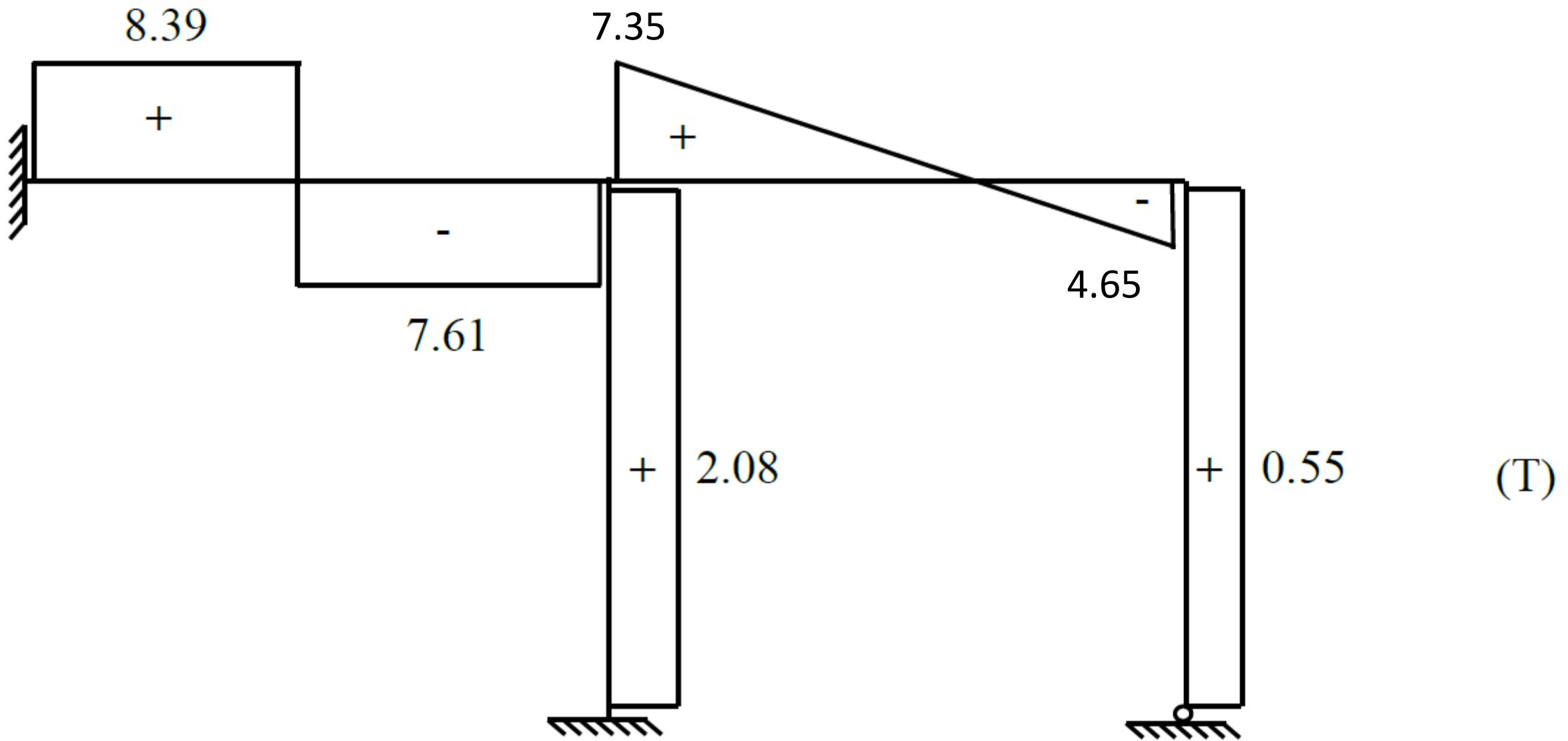
$$T_{21} = -8 + 0.39 = -7.61 \text{ t}$$

$$T_{23} = 6 + \frac{9.74 - 1.66}{6} = 7.35 \text{ t}$$

$$T_{32} = -6 + 1.35 = -4.65 \text{ t}$$

$$M = -9.74 + 7.35 \times 3.67 = 17.23 \text{ tm}$$

6. Kesme kuvveti diyagramı



21 çubuğu

$$\Delta\theta_2 = \frac{2.50}{m_{2\theta_2}^2} = \frac{1.25}{EI}, \quad \frac{-0.40}{2EI} = \frac{-0.2}{EI}, \quad \frac{-0.02}{2EI} = \frac{-0.01}{EI}$$

$$\hookrightarrow \frac{4EI}{L} = \frac{4E(4I)}{8} = 2EI$$

$$\theta_2 = \frac{1.25}{EI} - \frac{0.2}{EI} - \frac{0.01}{EI} = \frac{1.04}{EI}$$

23 çubuğu

$$\theta_2 = \frac{2.50 - 0.4 - 0.02}{2EI} = \frac{1.04}{EI}$$

Diagram of a beam structure with a fixed support at the left end and a roller support at the right end. The beam is divided into four segments by two internal supports. The segments are labeled (21), (24), (23), and (32) from left to right. The lengths of the segments are 0.25, 0.50, 0.25, and 0.667 respectively. The total length L is 1.66.

	1/2 ←	(21) 0.25	(24)	(23) 0.25	↔ 1/2	(32) 0.667	(35) 0.333
16.00		-16.00	0 0	6.00		-6.00	
1.25	←	2.50	5.00	2.50	→	1.25	
-0.20	←	-0.40	-0.79	-0.40	→	-0.20	
<u>-0.01</u>	←	<u>-0.02</u>	<u>-0.03</u>	<u>-0.02</u>	→	<u>0.13</u>	<u>0.07</u>
		17.04	-13.92	4.18	9.74		1.66
				2.50			
				-0.40			
				<u>-0.02</u>			
				2.08			

21 çubuğu

$$\Delta\theta_2 = \frac{2.50}{m_{2\theta_2}^2} = \frac{1.25}{EI}, \quad \frac{-0.40}{2EI} = \frac{-0.2}{EI}, \quad \frac{-0.02}{2EI} = \frac{-0.01}{EI}$$

$$\Rightarrow \frac{4EI}{L} = \frac{4E(4I)}{8} = 2EI$$

$$\theta_2 = \frac{1.25}{EI} - \frac{0.2}{EI} - \frac{0.01}{EI} = \frac{1.04}{EI}$$

23 çubuğu

$$\theta_2 = \frac{2.50 - 0.4 - 0.02}{2EI} = \frac{1.04}{EI}$$

		(21) 0.25	(24)	(23) 0.25		↔	1/2 0.667	(35) 0.333
16.00		-16.00	0 0	6.00			-6.00	
1.25	←	2.50	5.00	2.50	→	1.25		
-0.20	←	-0.40	-0.79	-0.40	→	-0.20		
				0.07	←	0.13	0.07	
					→	-0.01		
								1.66
				2.50				
				-0.40				
				-0.02				
					2.08			

24 çubuğu

$$\theta_2 = \frac{5.0 - 0.79 - 0.03}{4EI} = \frac{1.045}{EI}$$

32 çubuğu

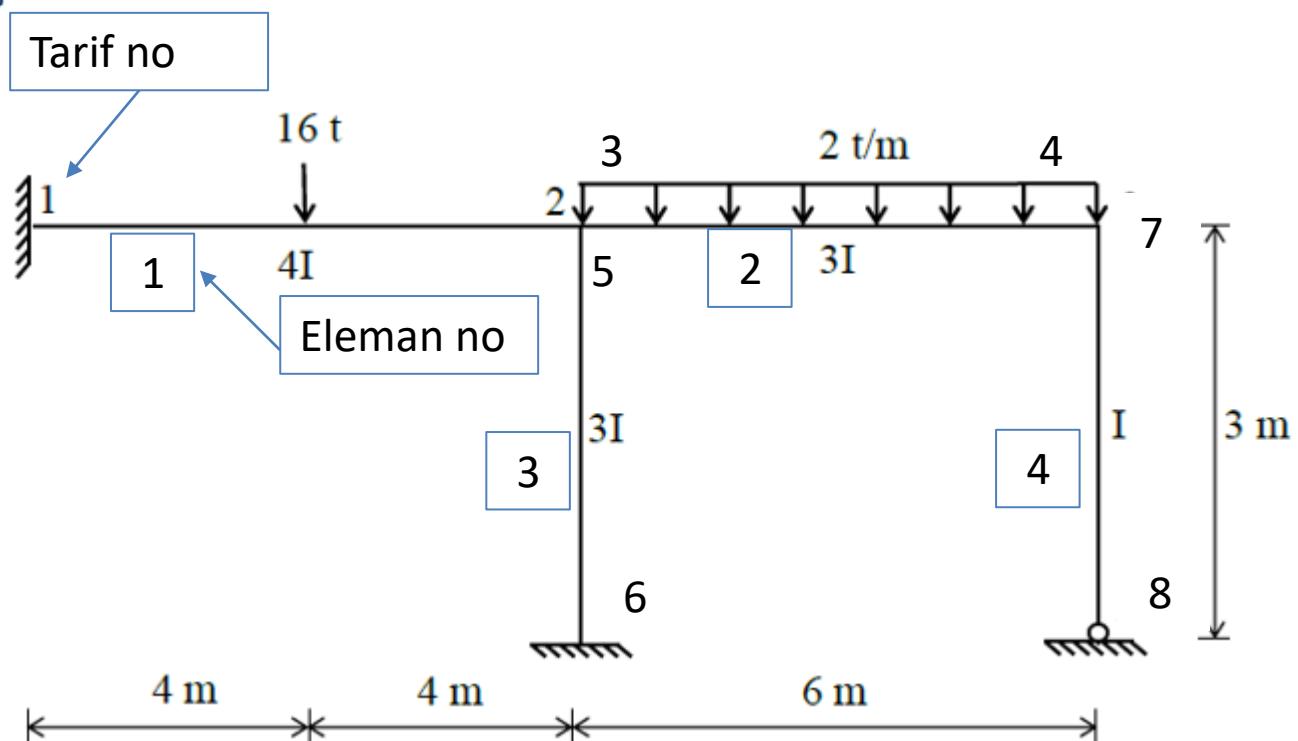
$$\theta_3 = \frac{3.17 + 0.13}{2EI} = \frac{1.65}{EI}$$

35 çubuğu

$$\theta_3 = \frac{1.59 + 0.07}{EI} = \frac{1.66}{EI}$$

V E R I D E G E R L E R I:

ELEMAN	BOY	ATALET MOM.	DAGITMA KATS
1	8.00	4.000	0.000
2	6.00	3.000	0.250
3	3.00	3.000	0.250
4	3.00	1.000	0.667
			0.500
			0.000
			0.333
			1.000



YUKLEME NO= 1

ITERASYON SAYISI=10

ELEMAN TARIF NO ANKAS.UC MOM. BAS.KI.I

1	1	-16.00	-8.00
	2	16.00	8.00
2	3	-6.00	-6.00
	4	6.00	6.00
3	5	0.00	0.00
	6	0.00	0.00
4	7	0.00	0.00
	8	0.00	0.00

H E S A P L A N A N D E G E R L E R:

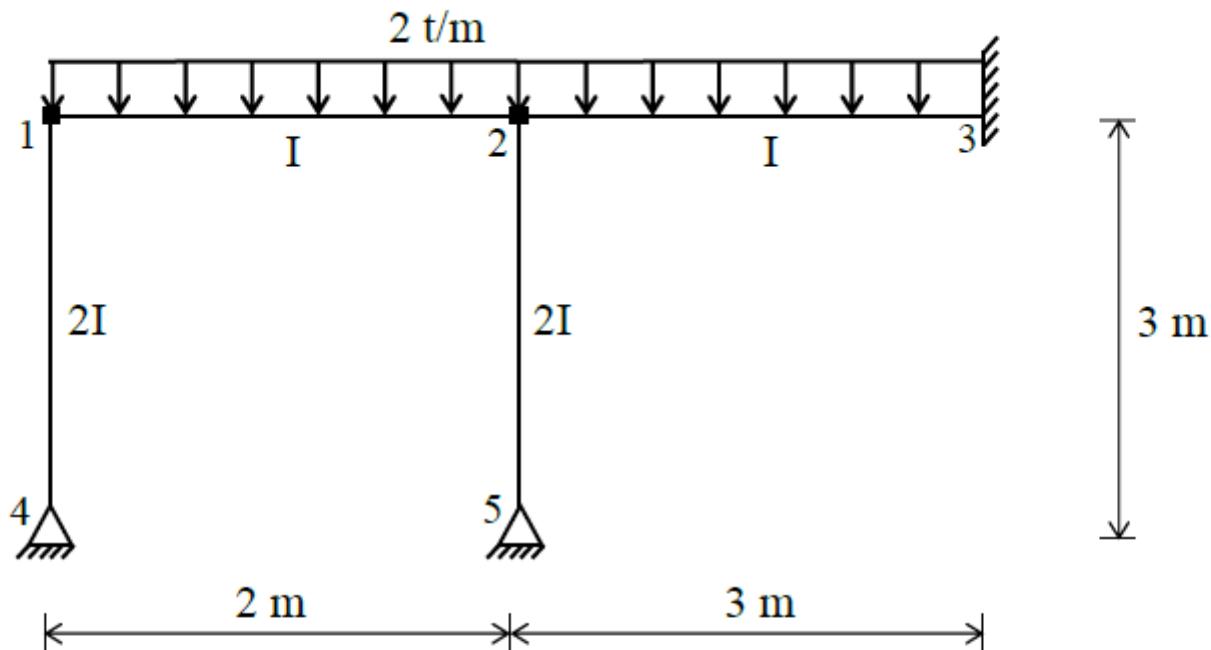
*** E L E M A N U C K U V V E T L E R I ***

ELEMAN	TARIF NO	MOMENT	KESME KUVVETI
1	1	-17.043	-8.391
	2	13.913	7.609
2	3	-9.739	-7.348
	4	1.652	4.652
3	5	-4.174	-2.087
	6	-2.087	-2.087
4	7	-1.652	-0.551
	8	0.000	-0.551

Xmax(i ucundan)= 4.000

1INCI ELEMAN ACIKLIK MOMENTI= 16.522

ÖRNEK- 3



Ankastrelik Momentler

$$M_{12} = -M_{21} = \frac{qL^2}{12} = \frac{2 \times 4}{12} = 0.667 \text{ tm}$$

$$M_{23} = -M_{32} = \frac{qL^2}{12} = \frac{2 \times 9}{12} = 1.5 \text{ tm}$$

1 düğümü

$$r_{12} = \frac{m_{1\theta_1}^{12}}{m_{1\theta_1}^{12} + m_{1\theta_1}^{14}} = \frac{\frac{4EI}{L}}{\frac{4EI}{L} + \frac{3EI}{L}} = \frac{\frac{4EI}{2}}{\frac{4EI}{2} + \frac{3E(2I)}{3}} = 0.5$$

$$r_{14} = \frac{m_{1\theta_1}^{14}}{m_{1\theta_1}^{14} + m_{1\theta_1}^{12}} = \frac{\frac{2EI}{4EI}}{\frac{2EI}{4EI}} = 0.5$$

$$r_{12} + r_{14} = 0.5 + 0.5 = 1$$

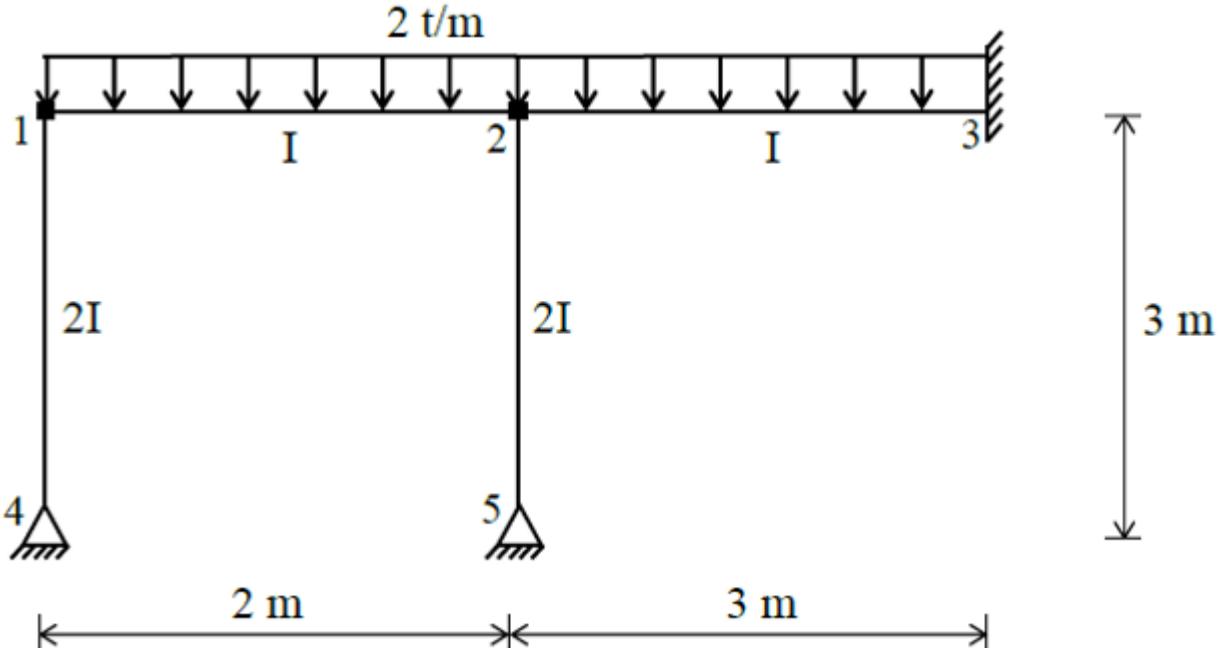
2 düğümü

$$r_{21} = \frac{m_{2\theta_2}^{21}}{m_{2\theta_2}^{21} + m_{2\theta_2}^{23} + m_{2\theta_2}^{25}} = \frac{\frac{4EI}{L}}{\frac{4EI}{L} + \frac{4EI}{L} + \frac{3EI}{L}} = \frac{\frac{4EI}{2}}{\frac{4EI}{2} + \frac{4EI}{3} + \frac{3E(2I)}{3}} = \frac{\frac{2EI}{5.333EI}}{\frac{2EI}{5.333EI}} = 0.375$$

$$r_{23} = \frac{1.333EI}{5.333EI} = 0.25$$

$$r_{25} = \frac{2EI}{5.333EI} = 0.375$$

$$r_{21} + r_{23} + r_{25} = 1.0$$



	(12)	\leftrightarrow 1/2	(21)		(23)	\rightarrow 1/2	
(14)	0.50		0.375		0.25		
0.50			0.375				
0.667		-0.667		1.5		-1.5	
-0.156	\leftarrow	-0.312	-0.312	-0.208	\rightarrow	-0.104	
-0.255	\rightarrow	-0.128					
-0.255							
0.024	\leftarrow	0.048	0.048	0.032	\rightarrow	0.016	
-0.012	\rightarrow	-0.006					
-0.012							
0.002		0.002	0.002	0.0015	\rightarrow	0.000	
-0.267	0.268		-1.063	-0.262	1.325		-1.588

Fark momentin büyük olduğu düğümden başlanır

$$2 \rightarrow -0.667 + 1.5 = 0.833$$

$$-0.833 \times 0.375 = -0.312$$

$$1 \rightarrow 0.667 - 0.156 = 0.511$$

$$-0.511 \times 0.5 = -0.255$$

$$\theta_1^{14} = \frac{-0.267}{\frac{3EI}{L}} = \frac{-0.267}{2EI} = -0.133/EI$$

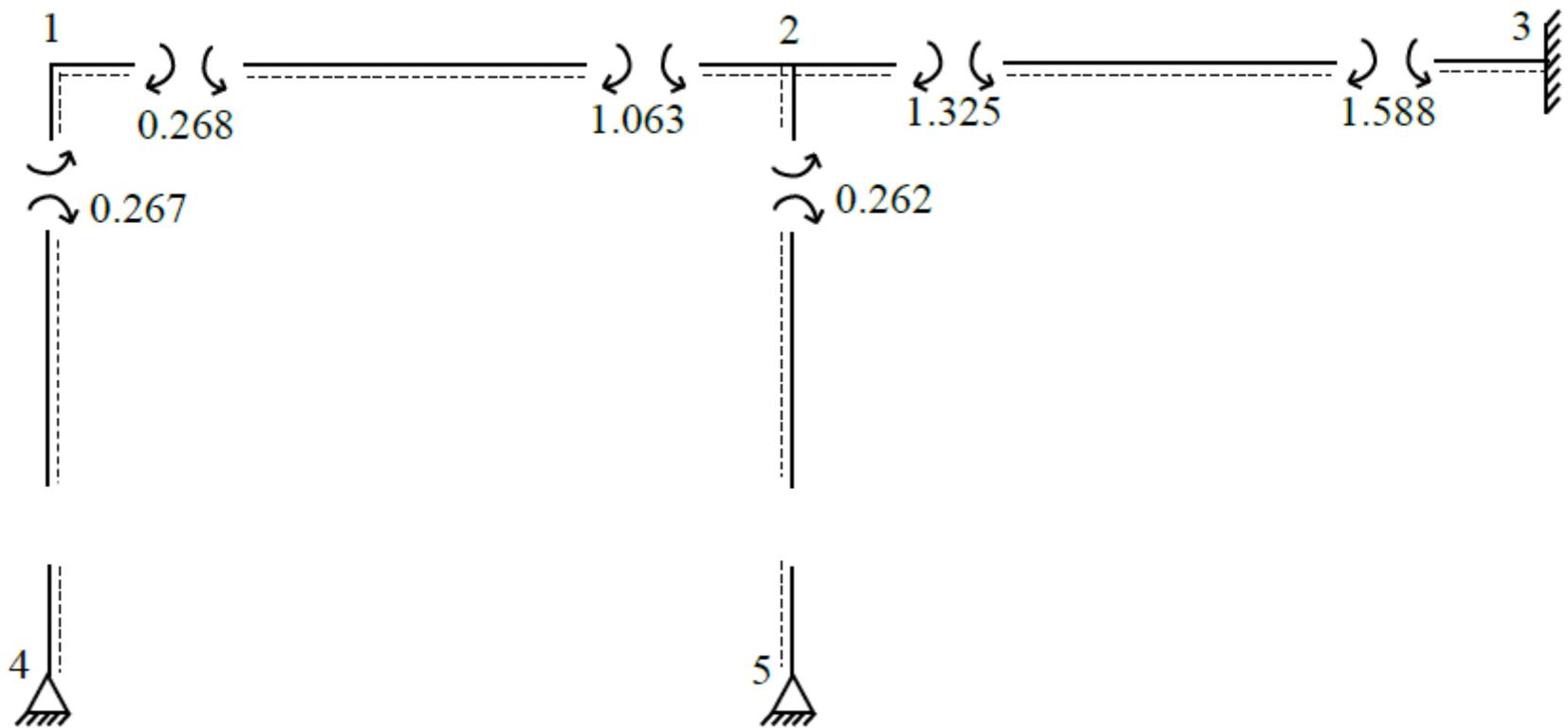
$$\theta_1^{12} = -0.133/EI$$

$$\theta_2^{21} = \frac{-0.312+0.048+0.002}{\frac{4EI}{L}} = \frac{-0.267}{2EI} = -0.131/EI$$

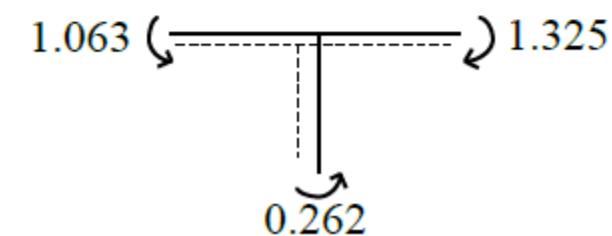
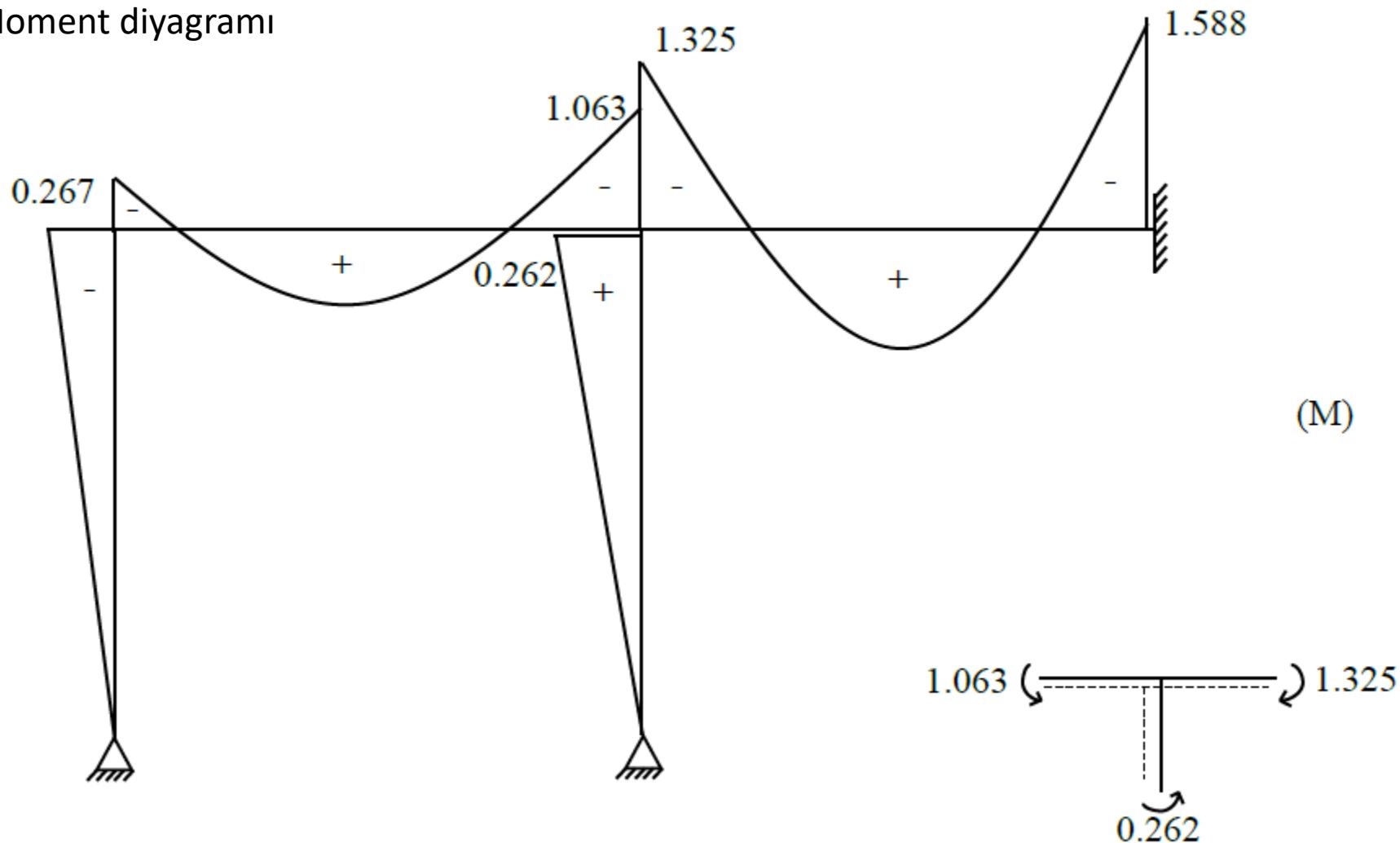
$$\theta_2^{25} = \frac{-0.312+0.048+0.002}{\frac{3EI}{L}} = \frac{-0.267}{2EI} = -0.131/EI$$

$$\theta_2^{23} = \frac{-0.208+0.032+0.0015}{\frac{4EI}{L}} = \frac{-0.1745}{1.333EI} = -0.131/EI$$

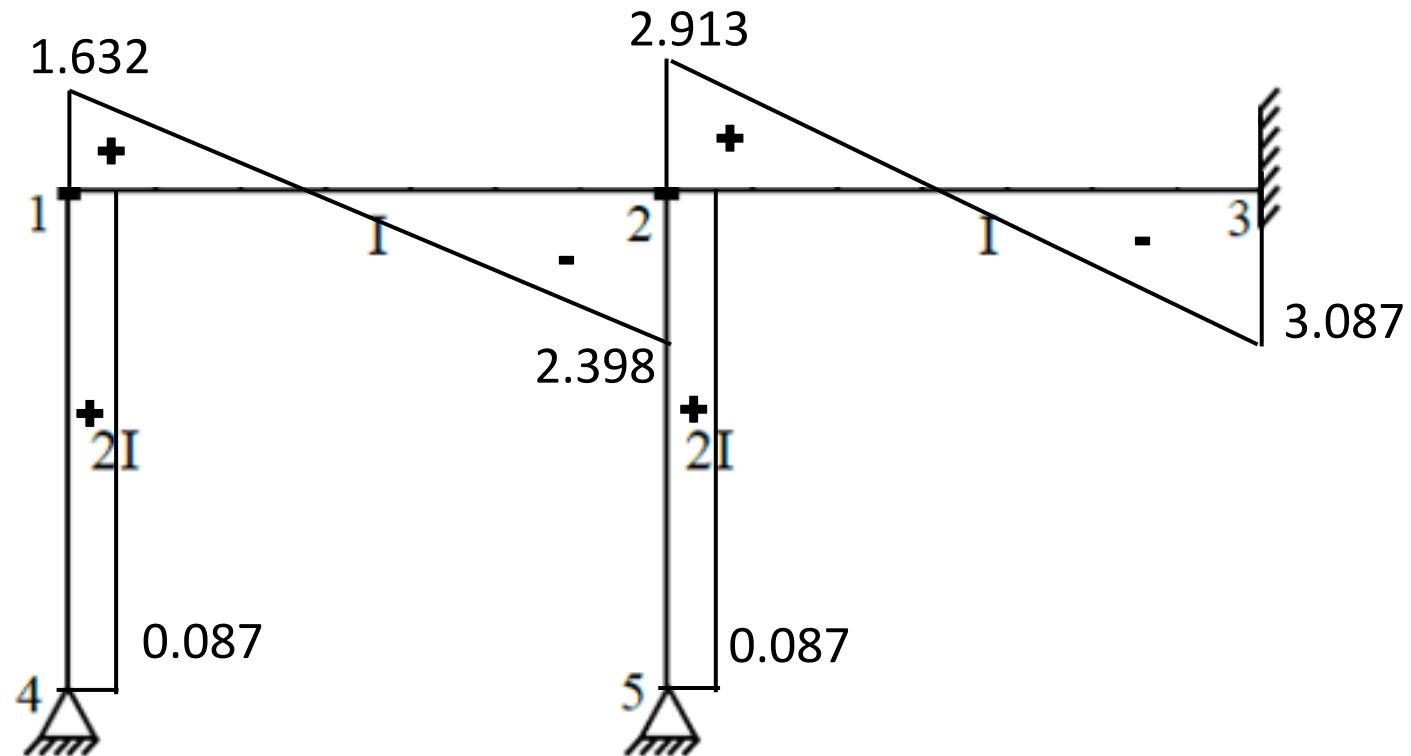
(14)	(12)	\leftrightarrow	1/2	(21)	(25)	(23)	\rightarrow	1/2
0.50	0.50			0.375	0.375	0.25		
	0.667			-0.667	1.5			-1.5
	-0.156	\leftarrow		-0.312	-0.208	\rightarrow		-0.104
-0.255	-0.255	\rightarrow		-0.128				
	0.024	\leftarrow		0.048	0.032	\rightarrow		0.016
	-0.012	\rightarrow		-0.006				
	-0.012			0.002	0.002	\rightarrow		0.000
				-1.063	-0.262	1.325		
								-1.588



Moment diyagramı



Kesme kuvveti diyagramı



CERCEVE

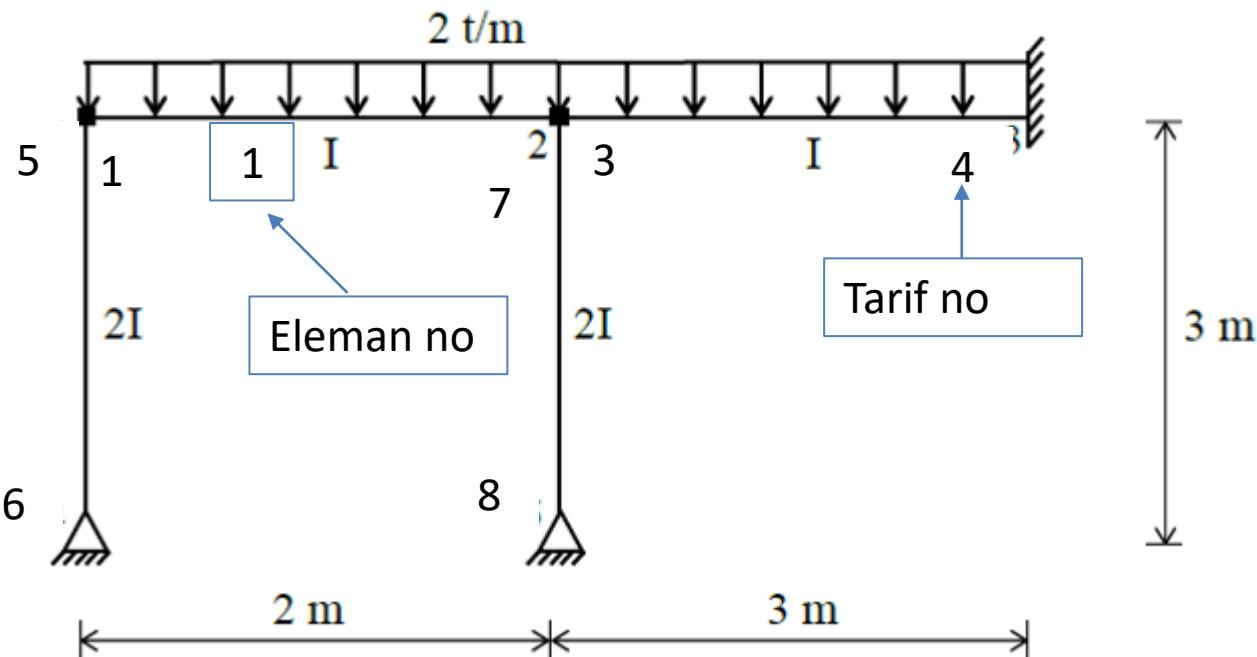
V E R I D E G E R L E R I:

ELEMAN	BOY	ATALET MOM.	DAGITMA	KATS
1	2.00	1.000	0.500	
			0.375	
2	3.00	1.000	0.250	
			0.000	
3	3.00	2.000	0.500	
			1.000	
4	3.00	2.000	0.375	
			1.000	

YUKLEME NO= 1

ITERASYON SAYISI=10

ELEMAN	TARIF NO	ANKAS.UC MOM.	BAS.KI.KESME K.
1	1	-0.67	-2.00
	2	0.67	2.00
2	3	-1.50	-3.00
	4	1.50	3.00
3	5	0.00	0.00
	6	0.00	0.00
4	7	0.00	0.00
	8	0.00	0.00



H E S A P L A N A N D E G E R L E R:

*** E L E M A N U C K U V V E T L E R I ***

ELEMAN	TARIF NO	MOMENT	KESME KUVVETI
1	1	-0.268	-1.602
	2	1.063	2.398
2	3	-1.325	-2.913
	4	1.587	3.087
3	5	0.268	0.089
	6	0.000	0.089
4	7	0.262	0.087
	8	0.000	0.087

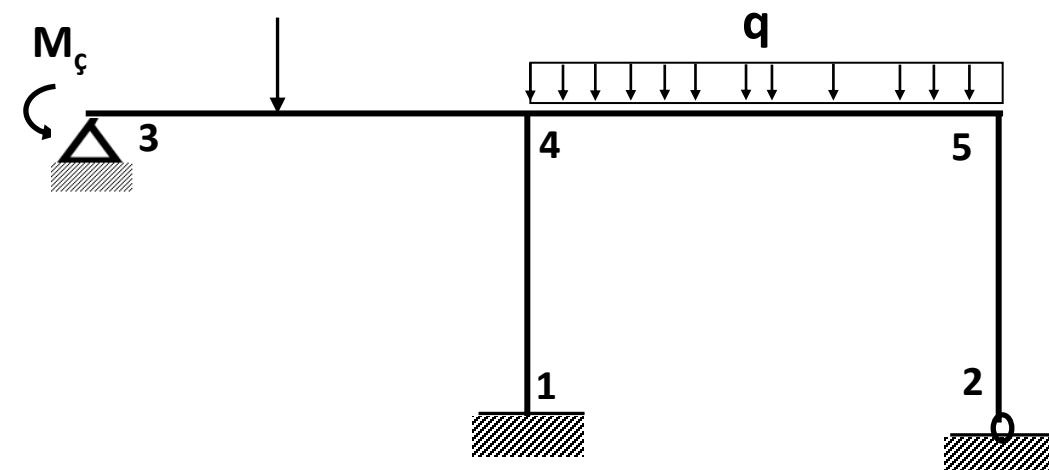
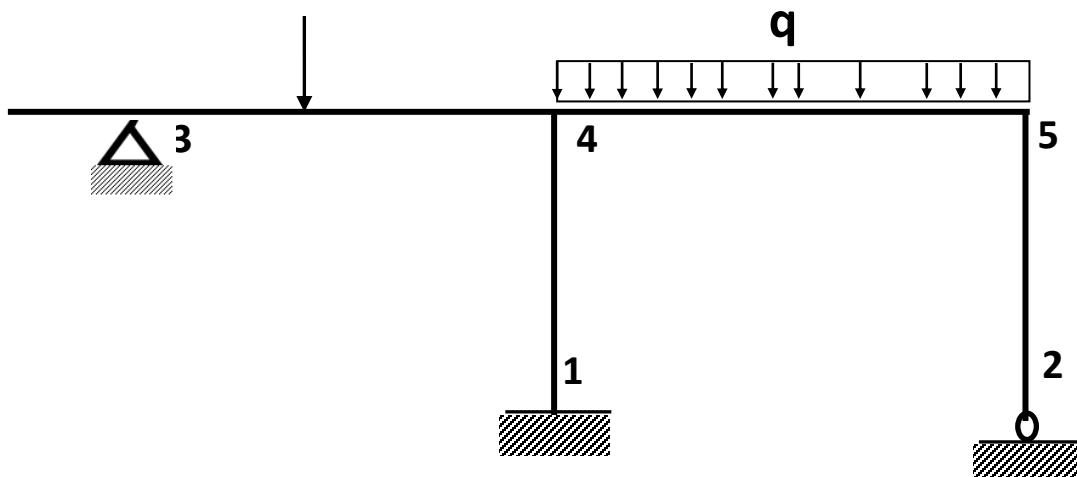
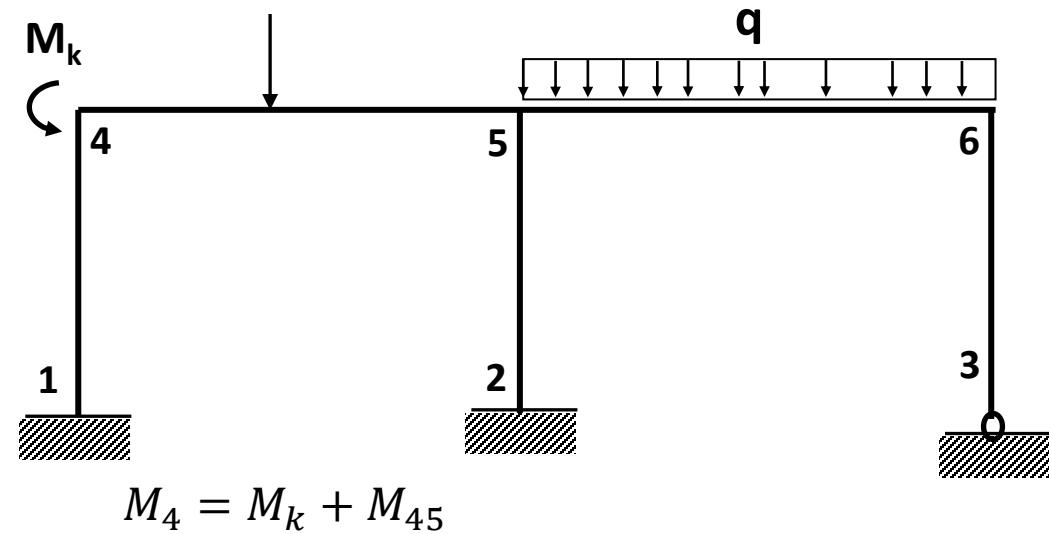
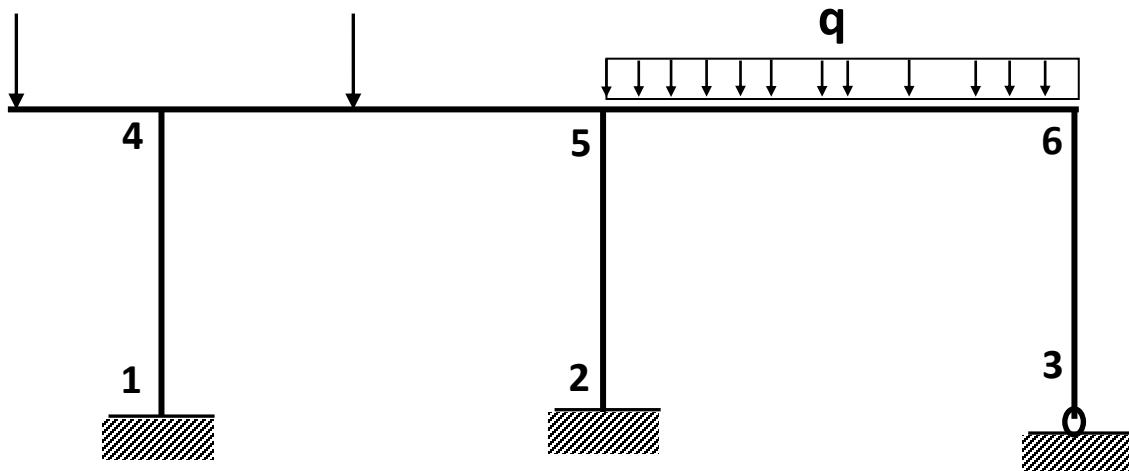
Xmax(i ucundan)= 0.801

1INCI ELEMAN ACIKLIK MOMENTI= 0.374

Xmax(i ucundan)= 1.456

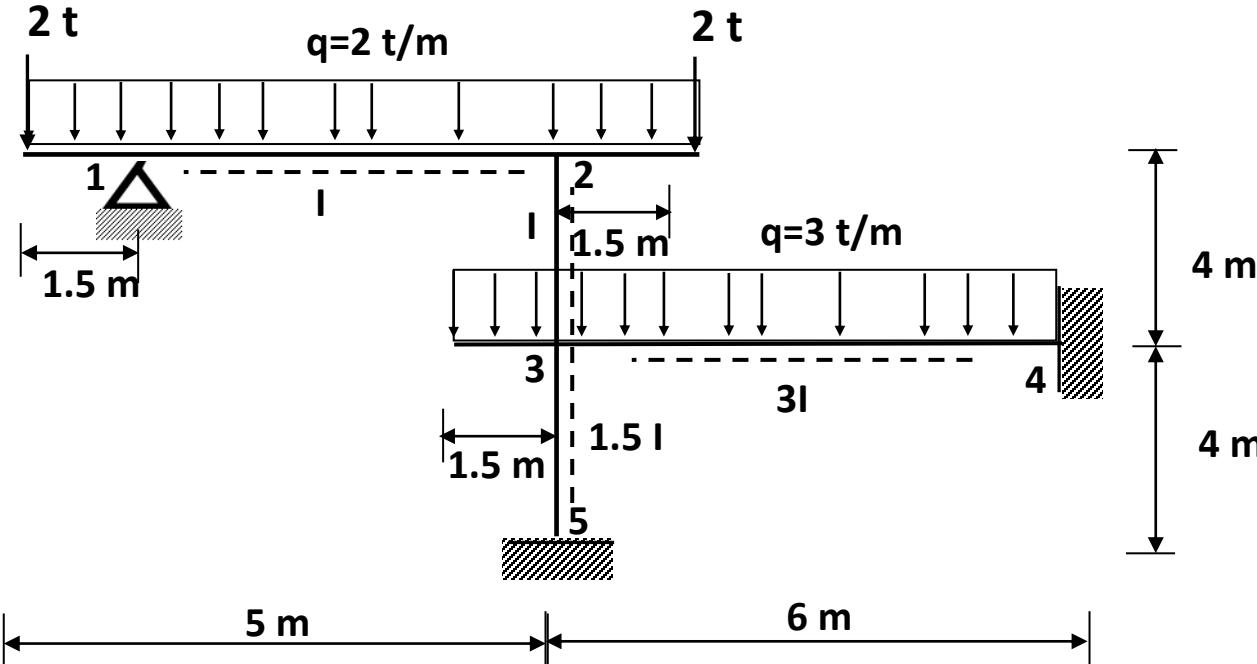
2INCI ELEMAN ACIKLIK MOMENTI= 0.796

KONSOLLU SİSTEMLER

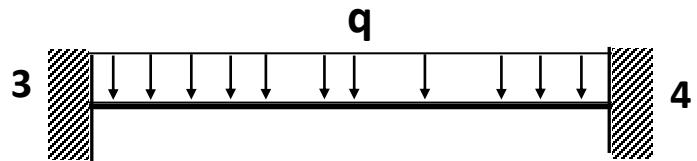


$$\bar{m}_{4\theta_4}^{43} = \frac{3EI}{L} \quad M_4 = \bar{\mathcal{M}}_{43} + \frac{M_c}{2} + M_{45}$$

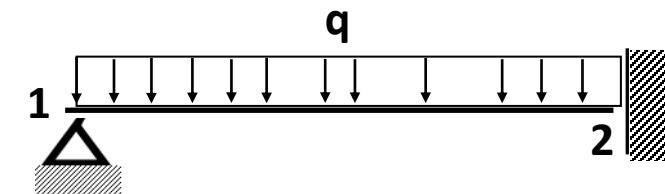
UYGULAMA 1



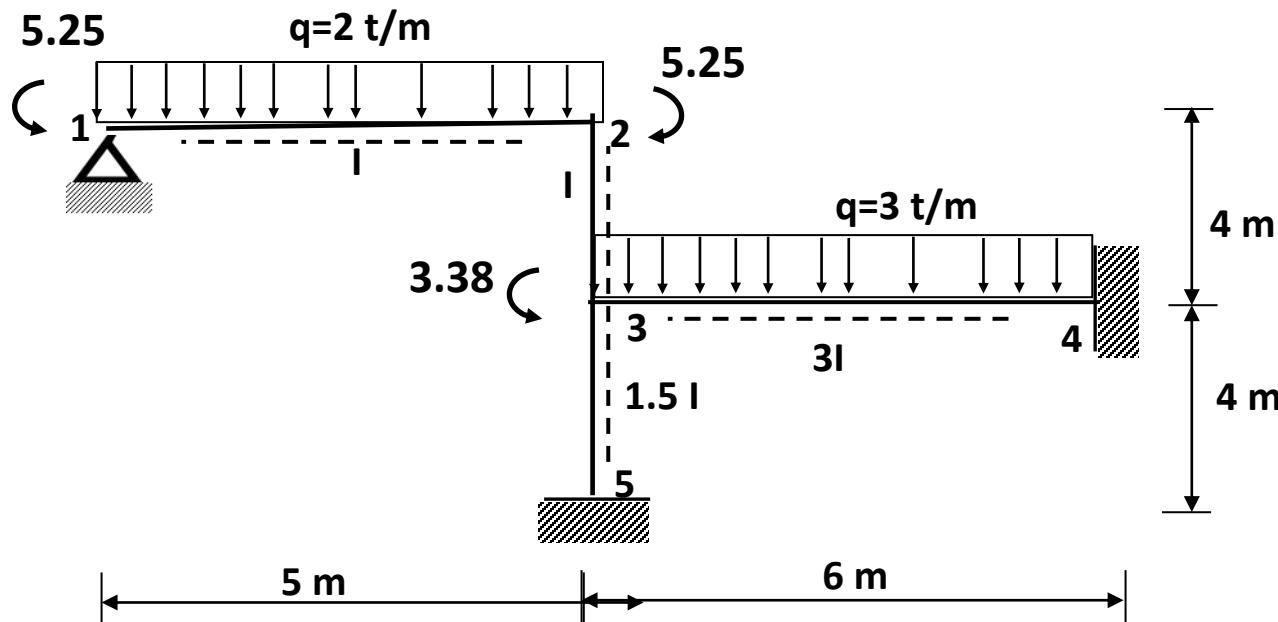
Cross metodunu kullanarak M N T diyagramlarını çiziniz.



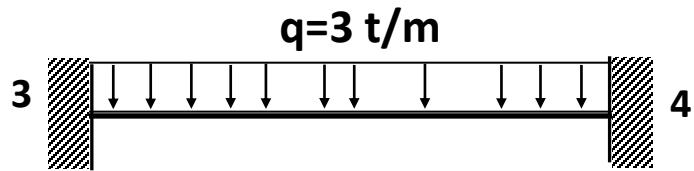
$$\mathcal{M}_{34} = -\mathcal{M}_{43} = \frac{qL^2}{12} = \frac{3 * 6^2}{12} = 9 \text{ tm}$$



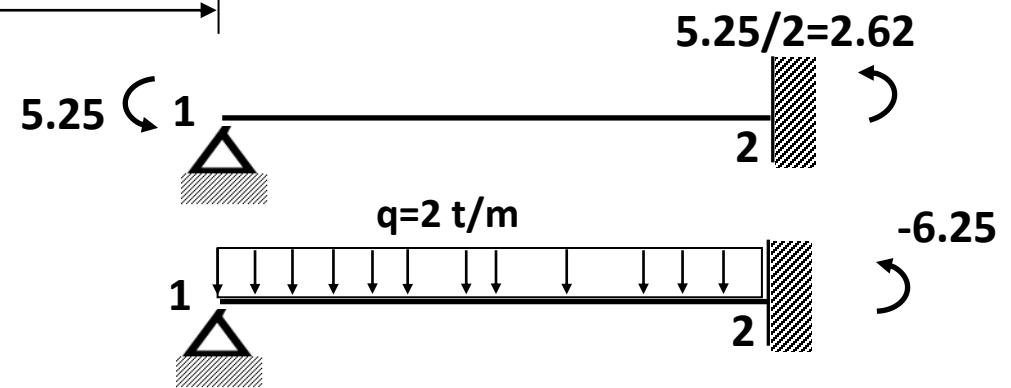
$$\mathcal{M}_{21} = -\frac{qL^2}{8} = -\frac{2 * 5^2}{8} = -6.25 \text{ tm}$$



1. Ankastrelilik üç momentleri:



$$\mathcal{M}_{34} = -\mathcal{M}_{43} = \frac{qL^2}{12} = \frac{3 * 6^2}{12} = 9 \text{ tm}$$



$$\bar{\mathcal{M}}_{21} = -\frac{qL^2}{8} = -\frac{2 * 5^2}{8} = -6.25 \text{ tm}$$

$$+2.62$$

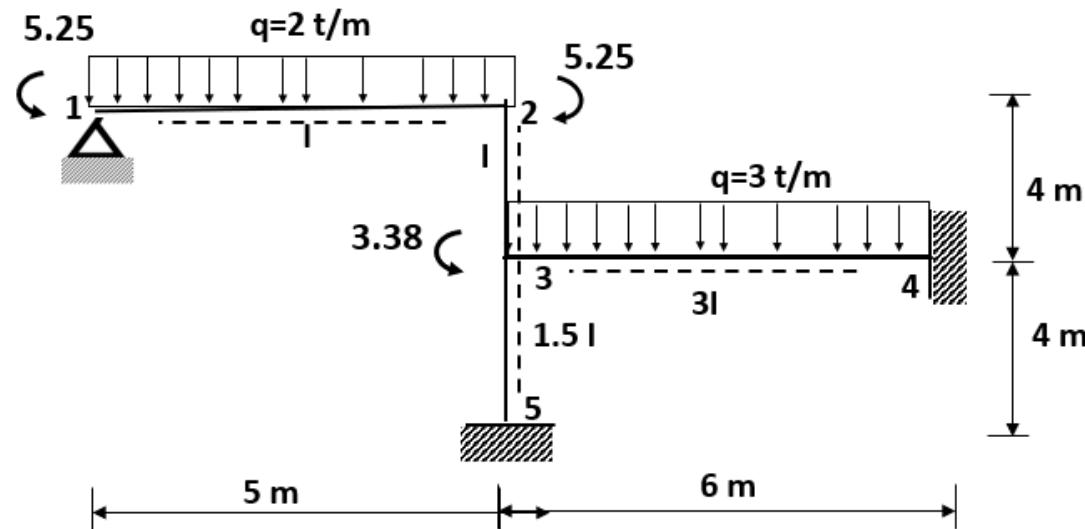
$$= -3.63$$

2. Dağıtma sayıları :

$$r_{21} = \frac{m_{2\theta_2}^{21}}{m_{2\theta_2}^{21} + m_{2\theta_2}^{23}} = \frac{\frac{3EI}{5}}{\frac{3EI}{5} + \frac{4EI}{4}} = \frac{0.6}{0.6 + 1.0} = 0.375$$

$$r_{23} = \frac{m_{2\theta_2}^{23}}{m_{2\theta_2}^{23} + m_{2\theta_2}^{21}} = \frac{\frac{4EI}{4}}{\frac{4EI}{4} + \frac{3EI}{5}} = \frac{1}{1.0 + 0.6} = 0.625$$

$$\sum r = 1 \text{ olmalı } \rightarrow 0.375 + 0.625 = 1 \quad \checkmark$$



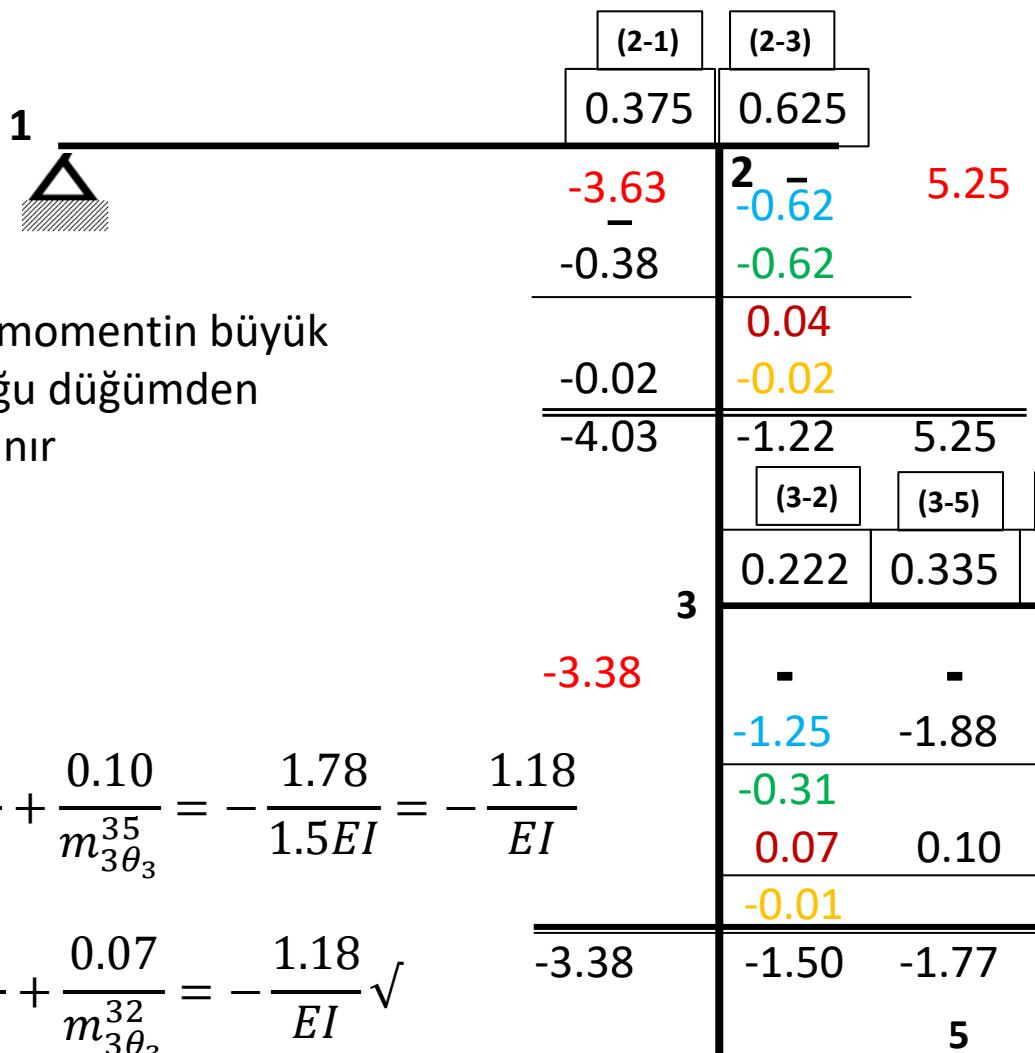
$$r_{32} = \frac{\frac{4EI}{4}}{\frac{4EI}{4} + \frac{4E3I}{6} + \frac{4E1.5I}{4}} = 0.222$$

$$r_{34} = \frac{\frac{4E3I}{6}}{\frac{4EI}{4} + \frac{4E3I}{6} + \frac{4E1.5I}{4}} = 0.445$$

$$r_{35} = \frac{\frac{4E1.5I}{6}}{\frac{4EI}{4} + \frac{4E3I}{6} + \frac{4E1.5I}{4}} = 0.333$$

$$\sum r = 1 \text{ olmalı } \rightarrow 0.222 + 0.445 + 0.333 = 1 \quad \checkmark$$

3. Dengeleme :



$$\theta_3 = -\frac{1.88}{m_{3\theta_3}^{35}} + \frac{0.10}{m_{3\theta_3}^{35}} = -\frac{1.78}{1.5EI} = -\frac{1.18}{EI}$$

$$\theta_3 = -\frac{1.25}{m_{3\theta_3}^{32}} + \frac{0.07}{m_{3\theta_3}^{32}} = -\frac{1.18}{EI} \checkmark$$

$$\theta_3 = -\frac{2.5}{m_{3\theta_3}^{34}} + \frac{0.14}{m_{3\theta_3}^{34}} = -\frac{2.36}{2EI} = -\frac{1.18}{EI} \checkmark$$

$$\theta_2 = -\frac{0.38}{m_{2\theta_2}^{21}} - \frac{0.02}{m_{2\theta_2}^{21}} = -\frac{0.40}{0.6EI} = -\frac{0.66}{EI}$$

$$\theta_2 = -\frac{0.62}{m_{2\theta_2}^{23}} - \frac{0.02}{m_{2\theta_2}^{23}} = -\frac{0.64}{EI} \approx \checkmark$$

3 düğümü

$$-3.38 + 9 = 5.62$$

$$-5.62 * 0.222 = -1.25$$

$$-5.62 * 0.335 = -1.88$$

$$-5.62 * 0.445 = -2.50$$

2 düğümü

$$-3.63 + 5.25 - 0.62 = 1.0$$

$$-1.0 * 0.375 = -0.38$$

$$-1.0 * 0.625 = -0.62$$

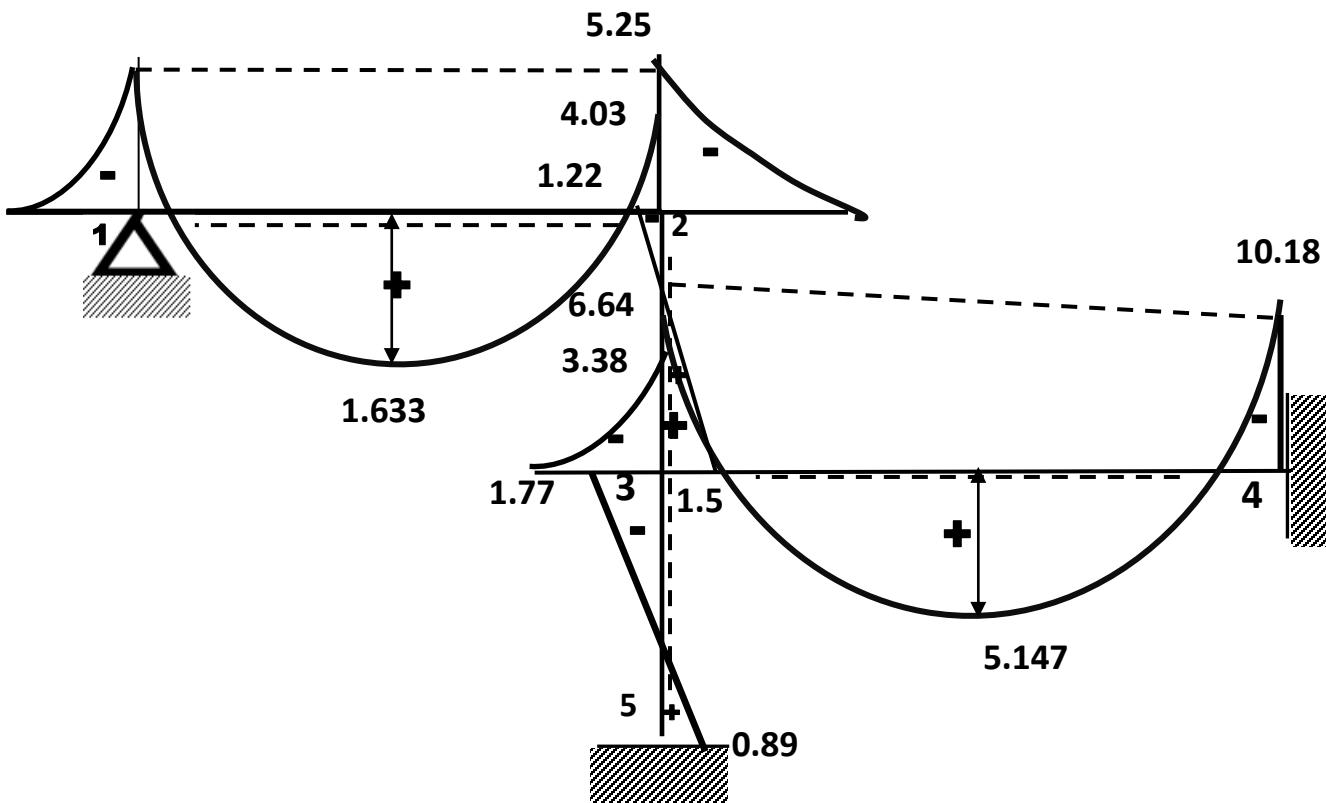
3 düğümü

$$-(-0.31) * 0.222 = 0.07$$

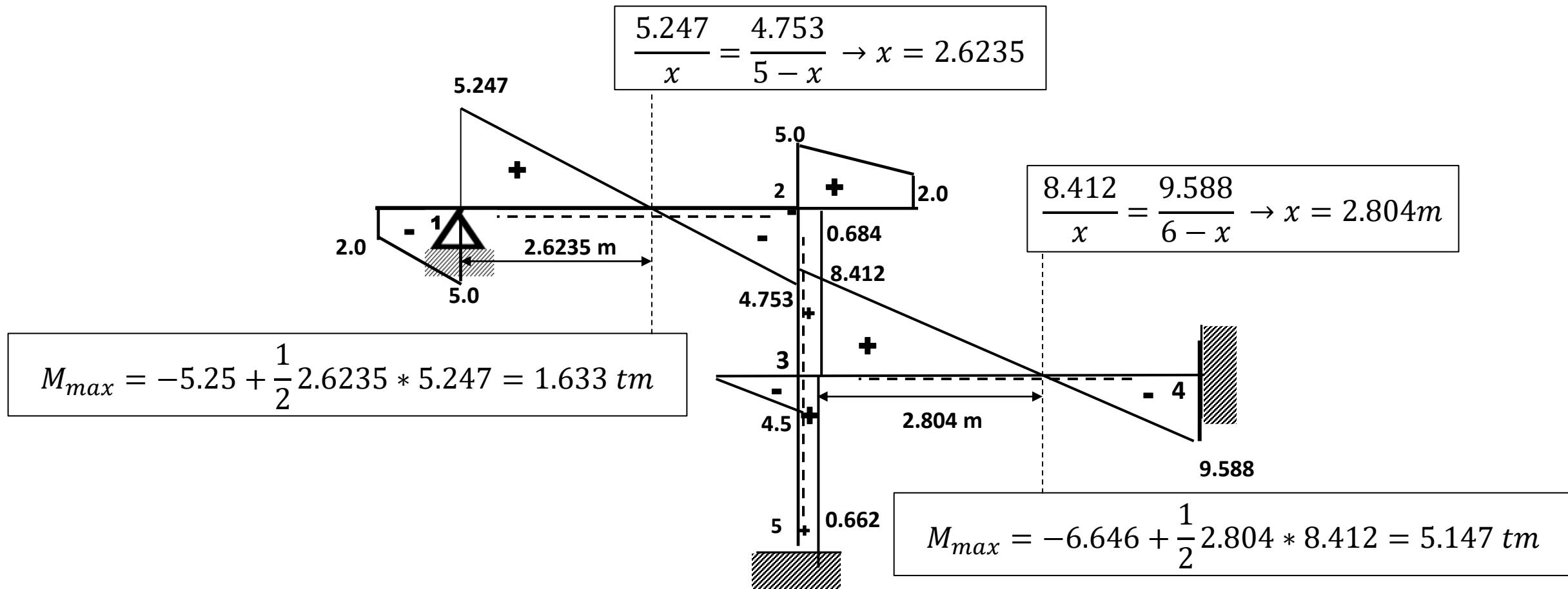
$$-(-0.31) * 0.335 = 0.10$$

$$-(-0.31) * 0.445 = 0.14$$

4. Moment diyagramı:



5. Kesme kuvveti diyagramı:



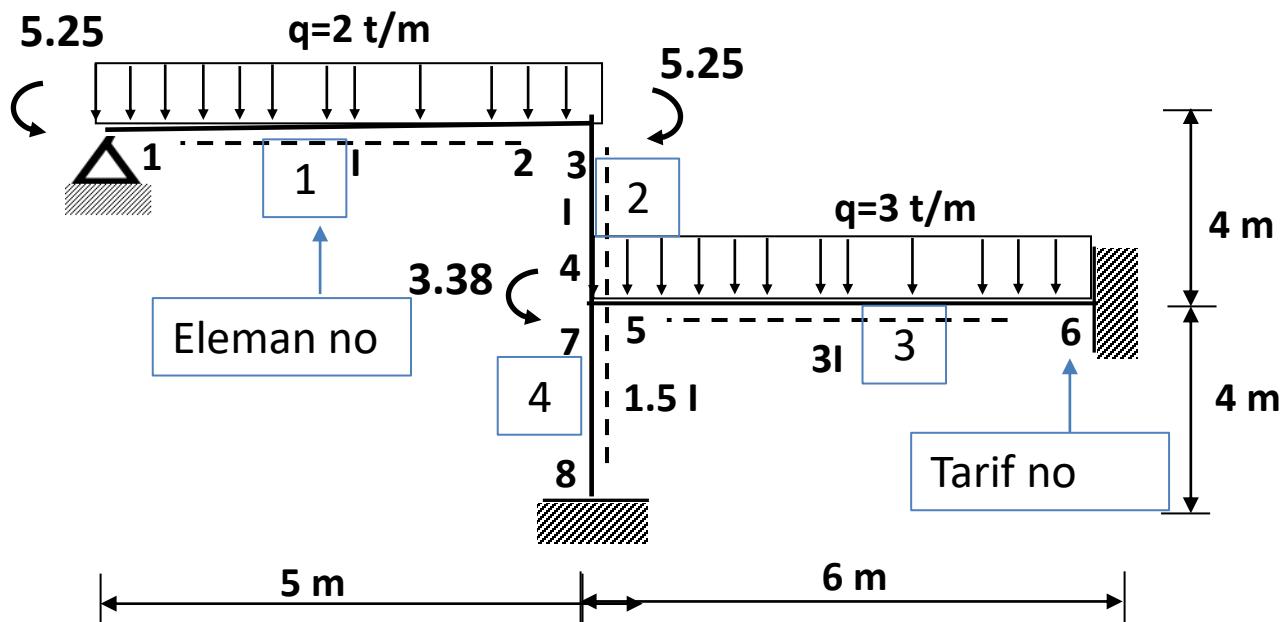
V E R I D E G E R L E R I:

ELEMAN	BOY	ATALET MOM.	DAGITMA KATS.
1	5.00	1.000	1.000 0.375
2	4.00	1.000	0.625 0.222
3	6.00	3.000	0.444 0.000
4	4.00	1.500	0.333 0.000

YUKLEME NO= 1

ITERASYON SAYISI=10

ELEMAN	TARIF NO	ANKAS.UC MOM.	BAS.KI.KESME K.
1	1	1.08	-5.00
	2	-1.08	5.00
2	3	0.00	0.00
	4	0.00	0.00
3	5	-5.62	-9.00
	6	9.00	9.00
4	7	0.00	0.00
	8	0.00	0.00



H E S A P L A N A N D E G E R L E R:

*** E L E M A N U C K U V V E T L E R I ***

ELEMAN	TARIF NO	MOMENT	KESME KUVVETI
1	1	-5.250	-5.247
	2	4.014	4.753
2	3	1.236	0.684
	4	1.501	0.684
3	5	-6.646	-8.412
	6	10.177	9.588
4	7	1.765	0.662
	8	0.883	0.662

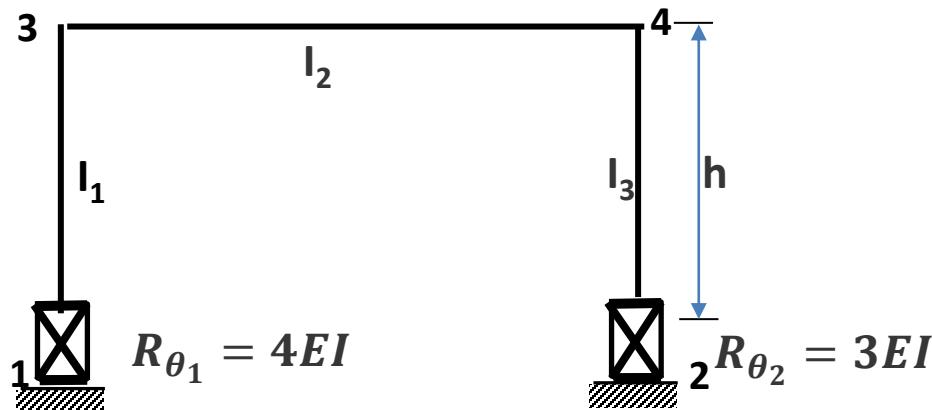
Xmax(i ucundan)= 2.624

1INCI ELEMAN ACIKLIK MOMENTI= 1.633

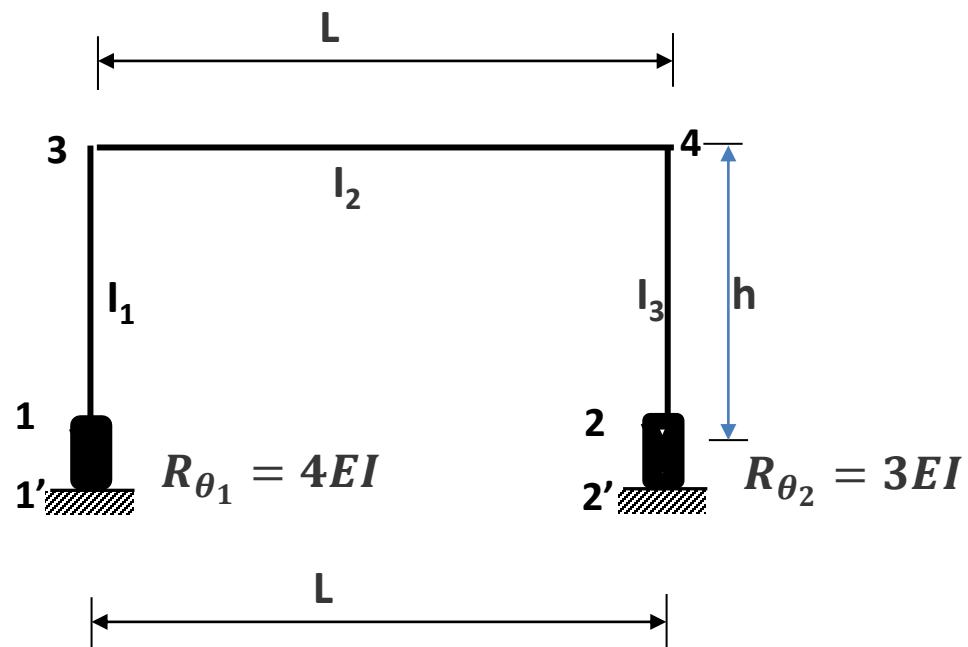
Xmax(i ucundan)= 2.804

3INCI ELEMAN ACIKLIK MOMENTI= 5.146

ELASTİK MESNETLİ SİSTEMLER



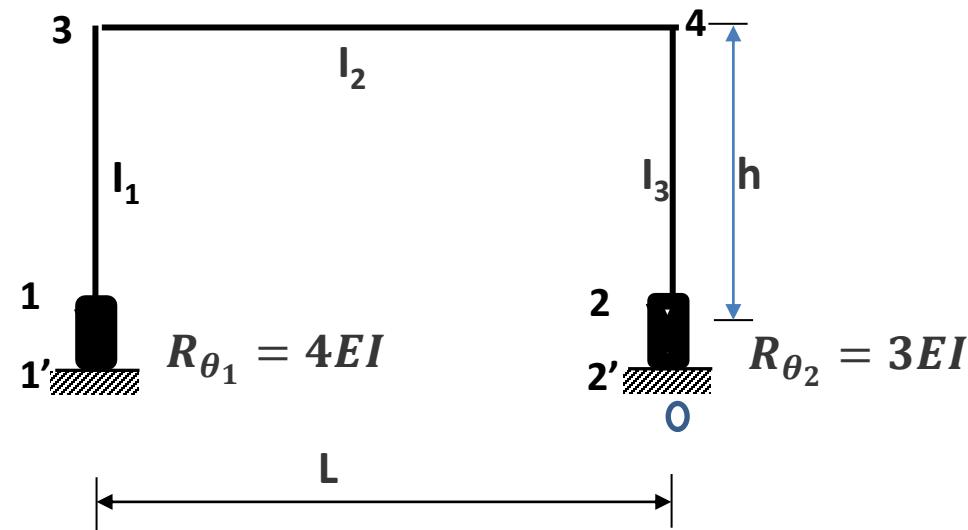
$$\frac{M}{\theta} = R_\theta \quad \theta = 1 \quad m_{i\theta_i} = M = R_\theta$$



$$r_{13} = \frac{m_{1\theta_1}^{13}}{m_{1\theta_1}^{13} + m_{1\theta_1}^{11'}} = \frac{\frac{4EI_1}{h}}{\frac{4EI_1}{h} + 4EI}$$

$$r_{11'} = \frac{m_{1\theta_1}^{11'}}{m_{1\theta_1}^{13} + m_{1\theta_1}^{11'}} = \frac{4EI}{\frac{4EI_1}{h} + 4EI}$$

$$m_{3\theta_3}^{31} = \frac{4EI_1}{h}$$



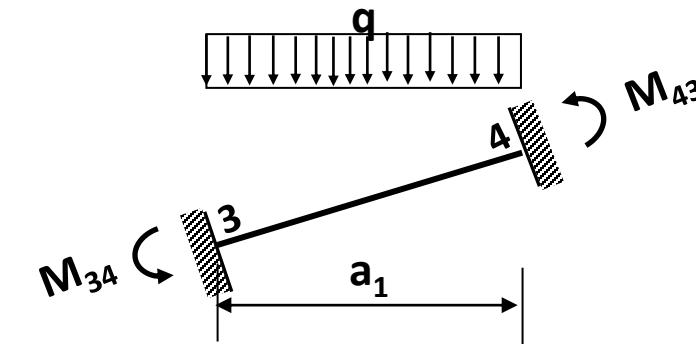
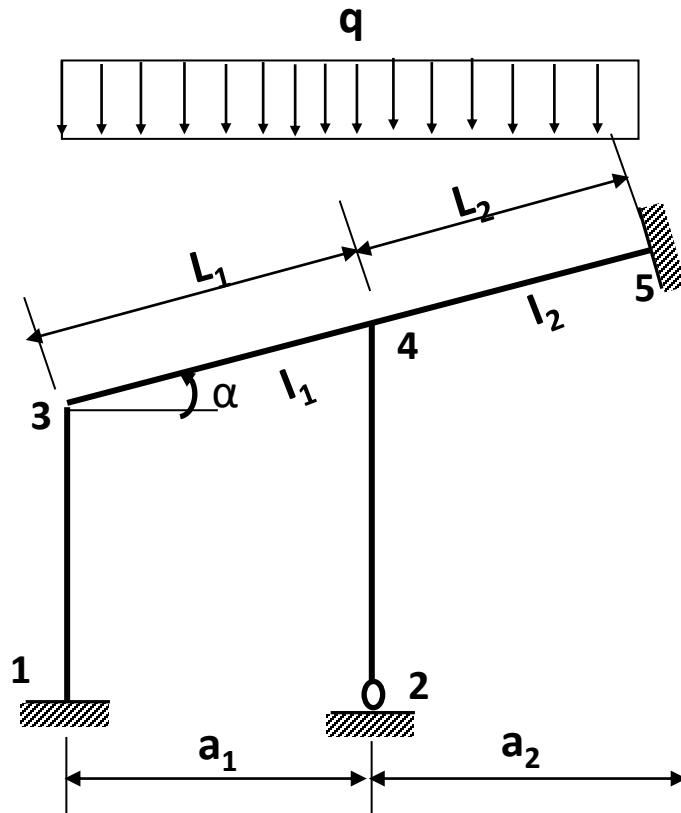
$$m_{3\theta_3}^{31} = \frac{4EI_1}{h}$$

$$r_{24} = \frac{m_{22}^{24}}{m_{2\theta_2}^{24} + m_{2\theta_2}^{22'}} = \frac{\frac{4EI_3}{h}}{\frac{4EI_3}{h} + 3EI}$$

$$r_{22'} = \frac{m_{2\theta_2}^{22'}}{m_{2\theta_2}^{24} + m_{2\theta_2}^{22'}} = \frac{3EI}{\frac{4EI_3}{h} + 3EI}$$

$$m_{4\theta_4}^{42} = \frac{4EI_3}{h}$$

Çubukları yatay ile açı yapan sistemler:



$$\mathcal{M}_{34} = -\mathcal{M}_{43} = \frac{q a_1^2}{12}$$

$$\mathcal{M}_{43} = -\mathcal{M}_{45} = \frac{q a_2^2}{12}$$

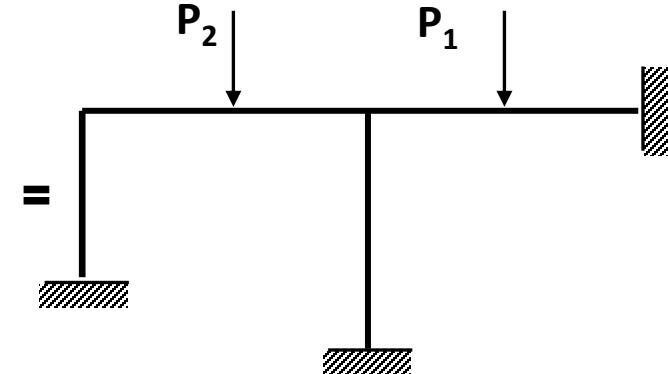
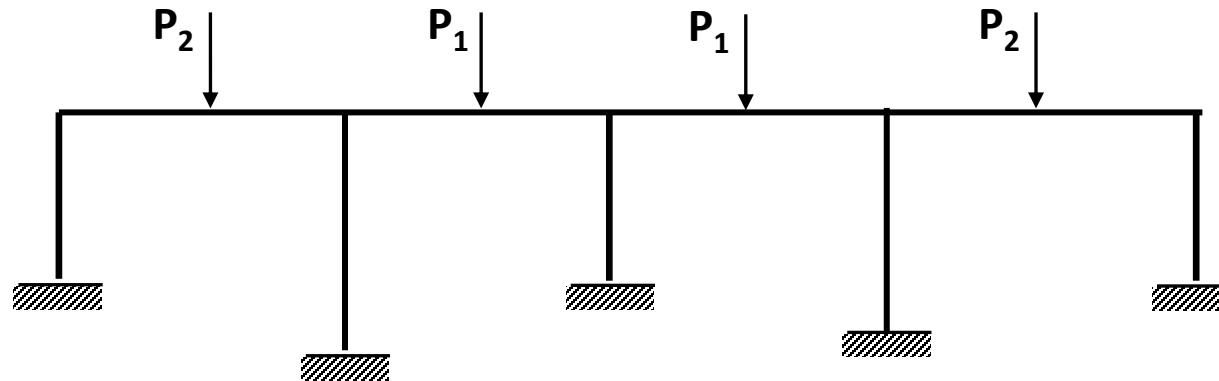
$$m_{3\theta_3}^{34} = \frac{4EI_1}{L_1} \quad m_{4\theta_{34}}^{45} = \frac{4EI_2}{L_2}$$

Ankastrelik momentleri hesaplanırken yatay mesafe alınır. Birim deplasman sabitleri hesaplanırken çubuk boyu göz önüne alınır.

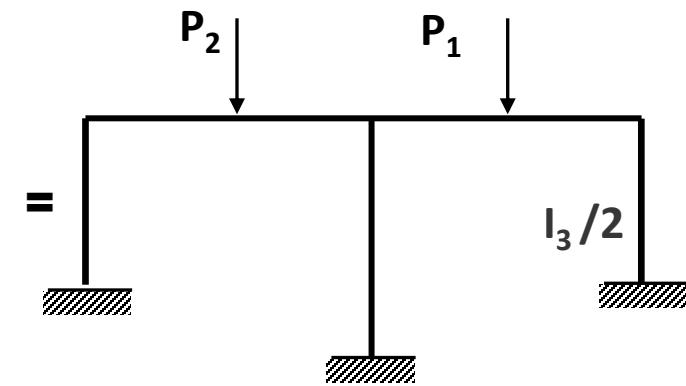
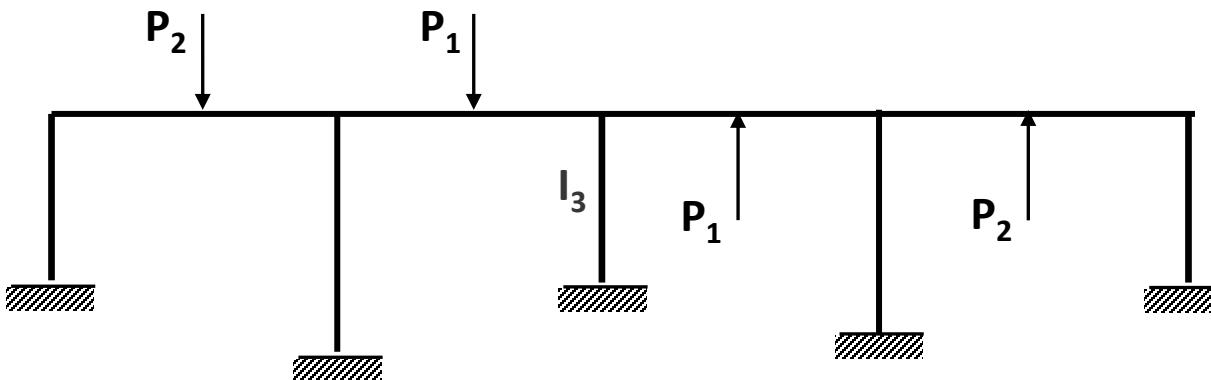
SİMETRİK VE ANTİMETRİK SİSTEMLER

1. Simetri ekseni üzerinde kolon bulunan sistemler

1.1 Simetrik yük hali

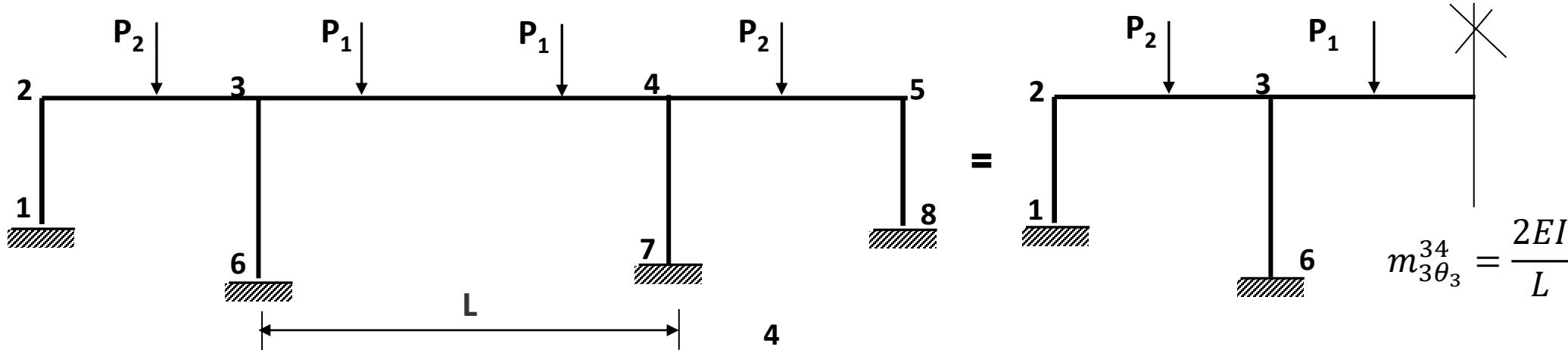


1.2 Antimetrik yükleme hali

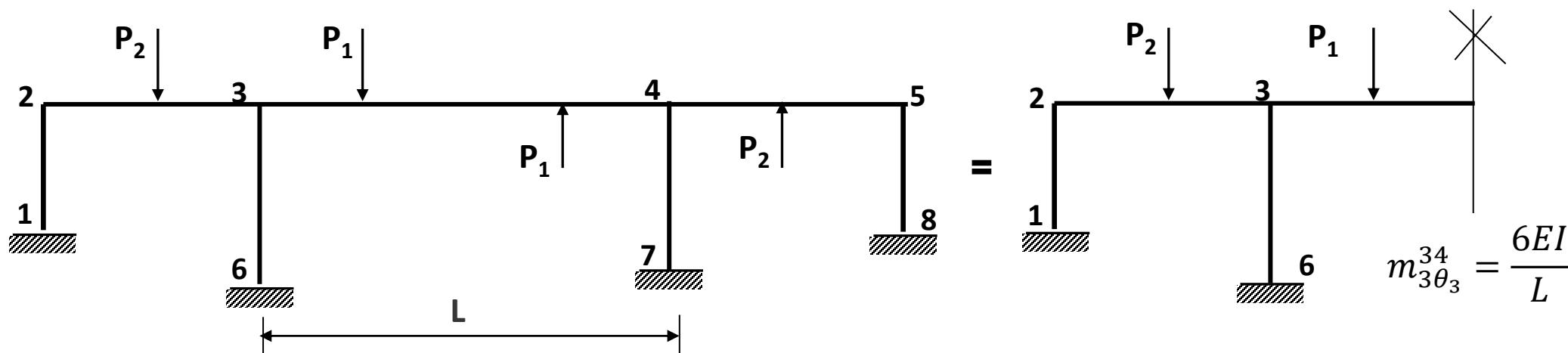


2. Simetri ekseni üzerinde kolon veya düğüm noktası bulunmayan elemanlar

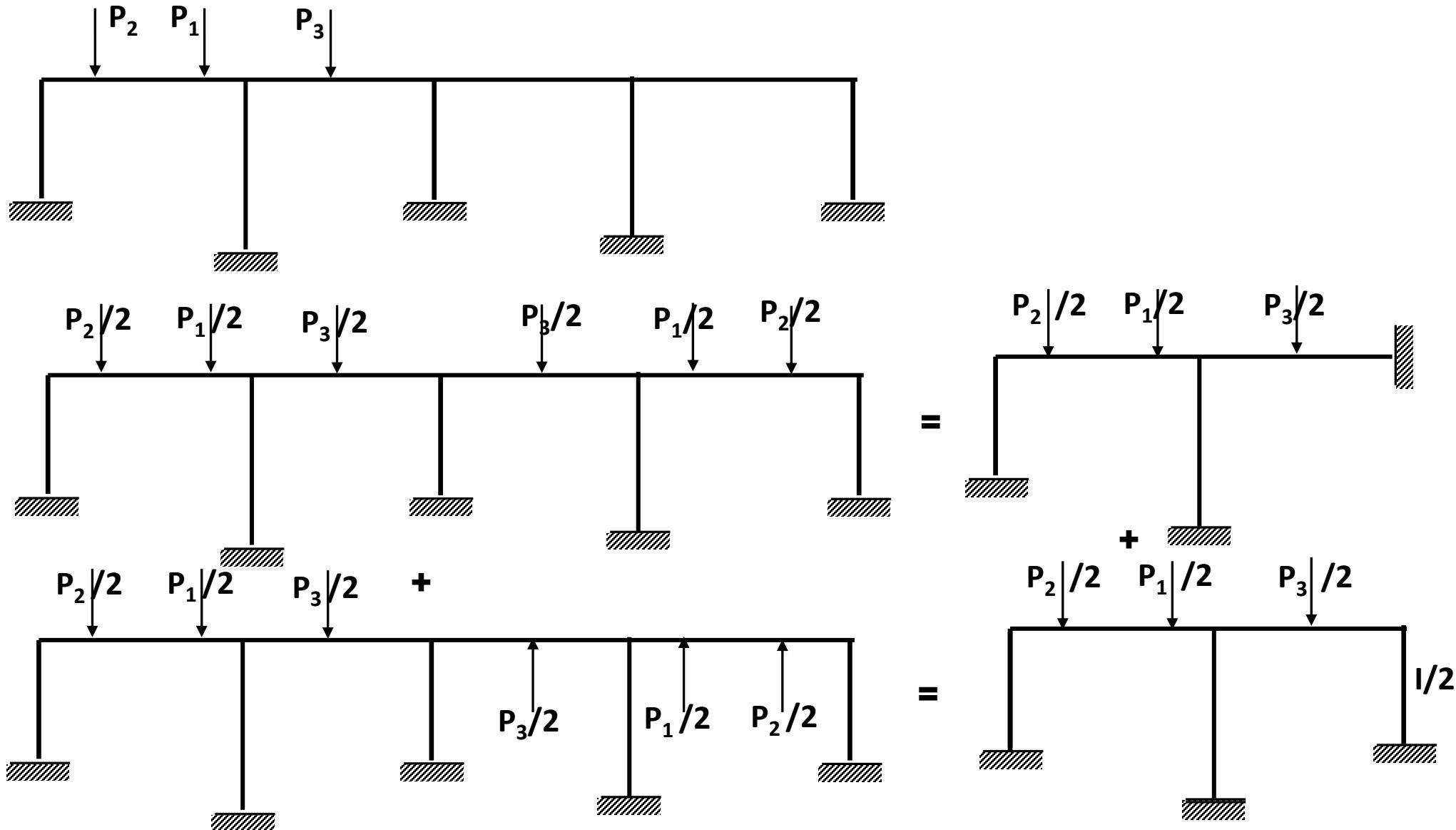
2.1 Simetrik yük hali



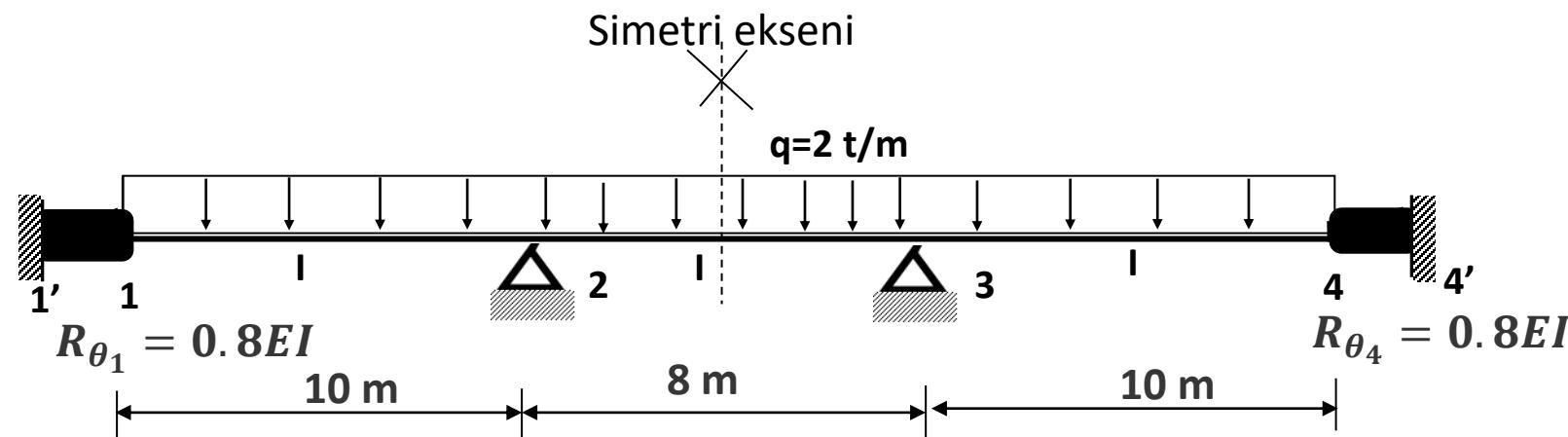
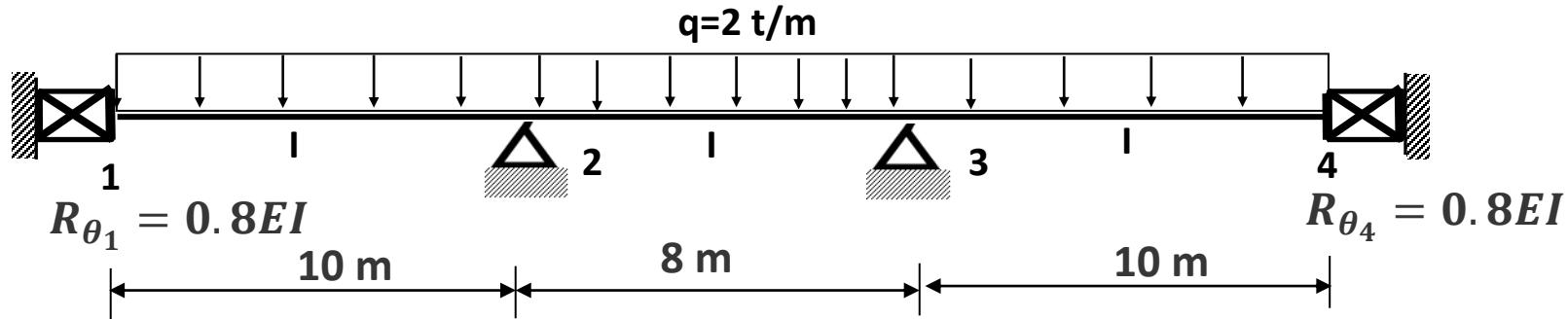
2.2 Antimetrik yük hali



3. Gelişmiş güzel yüklü simetrik sistemler

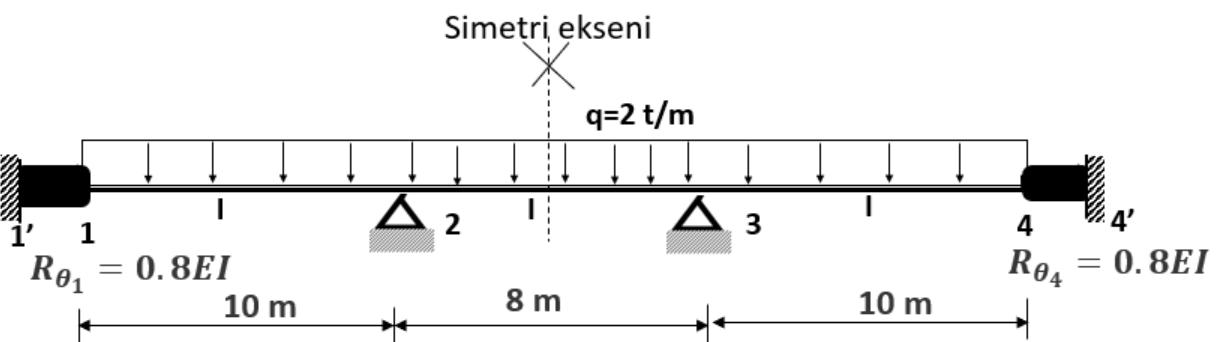


UYGULAMA 2



1. Ankastrelik momentleri:

$$\mathcal{M}_{12} = -\mathcal{M}_{21} = \frac{2 * 10^2}{12} = 16.67 \text{ tm}$$



$$\mathcal{M}_{23} = -\mathcal{M}_{32} = \frac{2 * 8^2}{12} = 10.67 \text{ tm}$$

$$\mathcal{M}_{34} = -\mathcal{M}_{43} = \frac{2 * 10^2}{12} = 16.67 \text{ tm}$$

2. Dağıtma sayıları:

$$r_{11'} = \frac{0.8EI}{0.8EI + \frac{4EI}{10}} = 0.667 \quad r_{12} = \frac{\frac{4EI}{10}}{0.8EI + \frac{4EI}{10}} = 0.333$$

$$r_{21} = \frac{\frac{4EI}{10}}{\frac{4EI}{10} + \frac{2EI}{8}} = 0.615 \quad r_{23} = \frac{\frac{2EI}{8}}{\frac{4EI}{10} + \frac{2EI}{8}} = 0.385$$



Simetri özelliğinden yarısı alınır

Simetri ekseni

$$q=2 \text{ t/m}$$

3. Cross dengemesi:

(1-1') (1-2)

0.667	0.333
-------	-------

$\frac{1}{2}$

(2-1) (2-3)

0.615	0.385
-------	-------

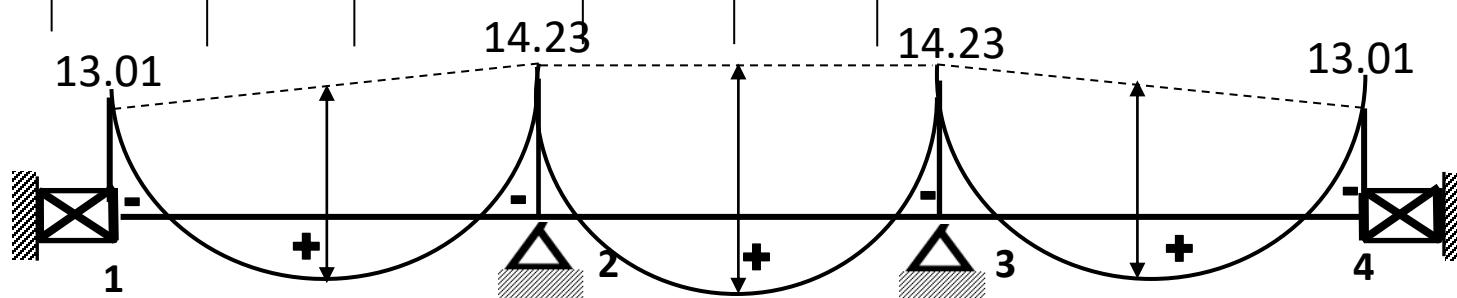


$$R_{\theta_1} = 0.8EI$$

$$R_{\theta_4} = 0.8EI$$

	16.67
-11.12	-5.65
	2.70
-1.80	-0.90
	0.14
-0.09	-0.05
	13.01
-13.01	

	-16.67
	-2.78
0.615	5.40
	3.38
	-0.45
	0.28
	0.17
	-0.03
	0.02
	0.01
	-14.23
	14.23

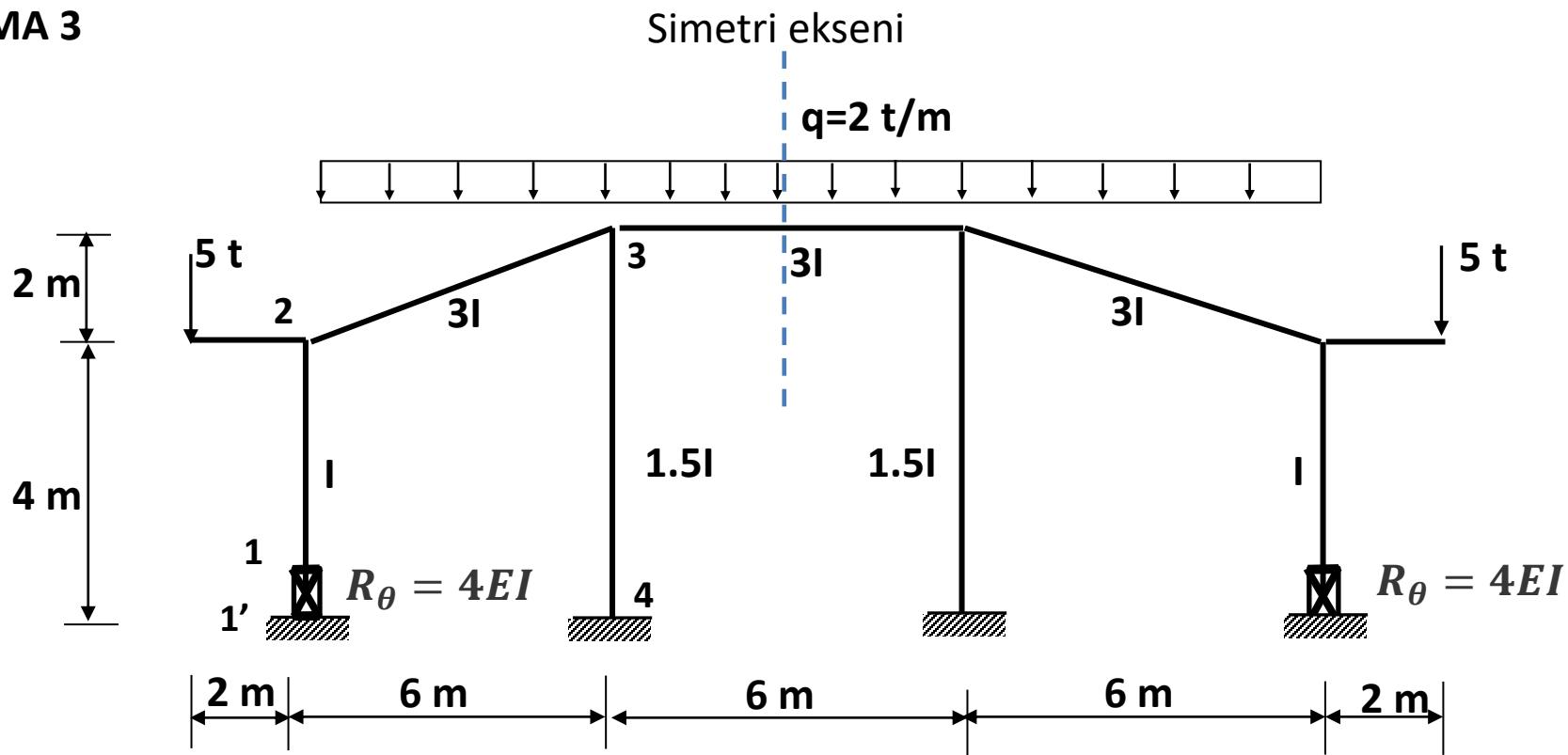


$$\frac{qL^2}{8} = \frac{2 * 8^2}{8} = 16 \text{ tm}$$

$$\frac{qL^2}{8} = \frac{2 * 10^2}{8} = 25 \text{ tm}$$

4. Moment diyagramı:

UYGULAMA 3



1. Ankastrelik momentleri:

$$\mathcal{M}_{23} = -\mathcal{M}_{32} = \frac{2 * 6^2}{12} = 6 \text{ tm} \quad \mathcal{M}_{33'} = \mathcal{M}_{3'3} - \frac{2 * 6^2}{12} = 6 \text{ tm} \quad M_{2_{konsol}} = -2 * 5 = -10 \text{ tm}$$

2. Birim deplasman sabitleri

$$m_{1\theta_1}^{12} = \frac{4EI}{L} = \frac{4EI}{4} = EI \quad m_{1\theta_1}^{11'} = 4EI \quad m_{2\theta_2}^{21} = \frac{4EI}{L} = \frac{4EI}{4} = EI \quad m_{2\theta_2}^{23} = \frac{4EI}{L} = \frac{4E3I}{6.32} = 1.9EI$$

$$m_{3\theta_3}^{32} = 1.9EI \quad m_{3\theta_3}^{33'} = \frac{2E3I}{6} = EI \quad m_{3\theta_3}^{34} = \frac{4E1.5I}{6} = EI$$

2. Dağıtma sayıları

$$r_{12} = \frac{EI}{EI + 4EI} = 0.20 \quad r_{11'} = \frac{4EI}{EI + 4EI} = 0.80 \quad r_{12} + r_{11'} = 1 \rightarrow 0.20 + 0.80 = 1.0 \checkmark$$

$$r_{21} = \frac{EI}{EI + 1.9EI} = 0.35 \quad r_{23} = \frac{1.9EI}{EI + 1.9EI} = 0.65 \quad r_{21} + r_{23} = 1 \rightarrow 0.35 + 0.65 = 1.0 \checkmark$$

$$r_{32} = \frac{1.9EI}{1.9EI + EI + EI} = 0.50 \quad r_{33'} = \frac{EI}{1.9EI + EI + EI} = 0.25 \quad r_{34} = 0.25 \quad r_{32} + r_{33'} + r_{34} = 1 \checkmark$$

3. Cross dengelemesi

		(2-3)		(3-2)		(3-4)		(3-3')	
		0.65		0.50		0.25		0.25	
	(2-1)	0.35			-6.00				
-10.00		6.00		1.30				6.00	
1.40		2.60		-0.65		-0.33		-0.32	
				0.10					
				-0.05		-0.025		-0.025	
0.12		0.21		0.71		0.35		-0.35	
				-5.30		0.33		5.65	
-0.02									
0.01		0.01							
1.52		8.48							
(1-2)		(1-1')							
0.20		0.80							
0.70									
-0.14		0.56							
0.06									
0.01		0.05							
0.64		-0.61							

1/2

1/2

(4-3)

-0.16

-0.02

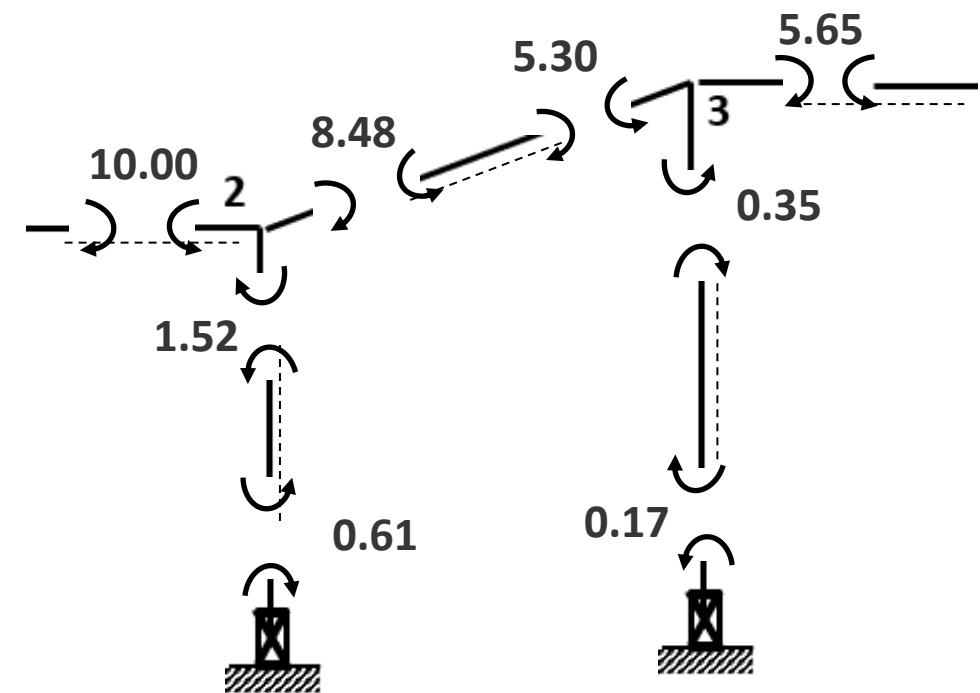
-0.18

3. Cross dengelemesi

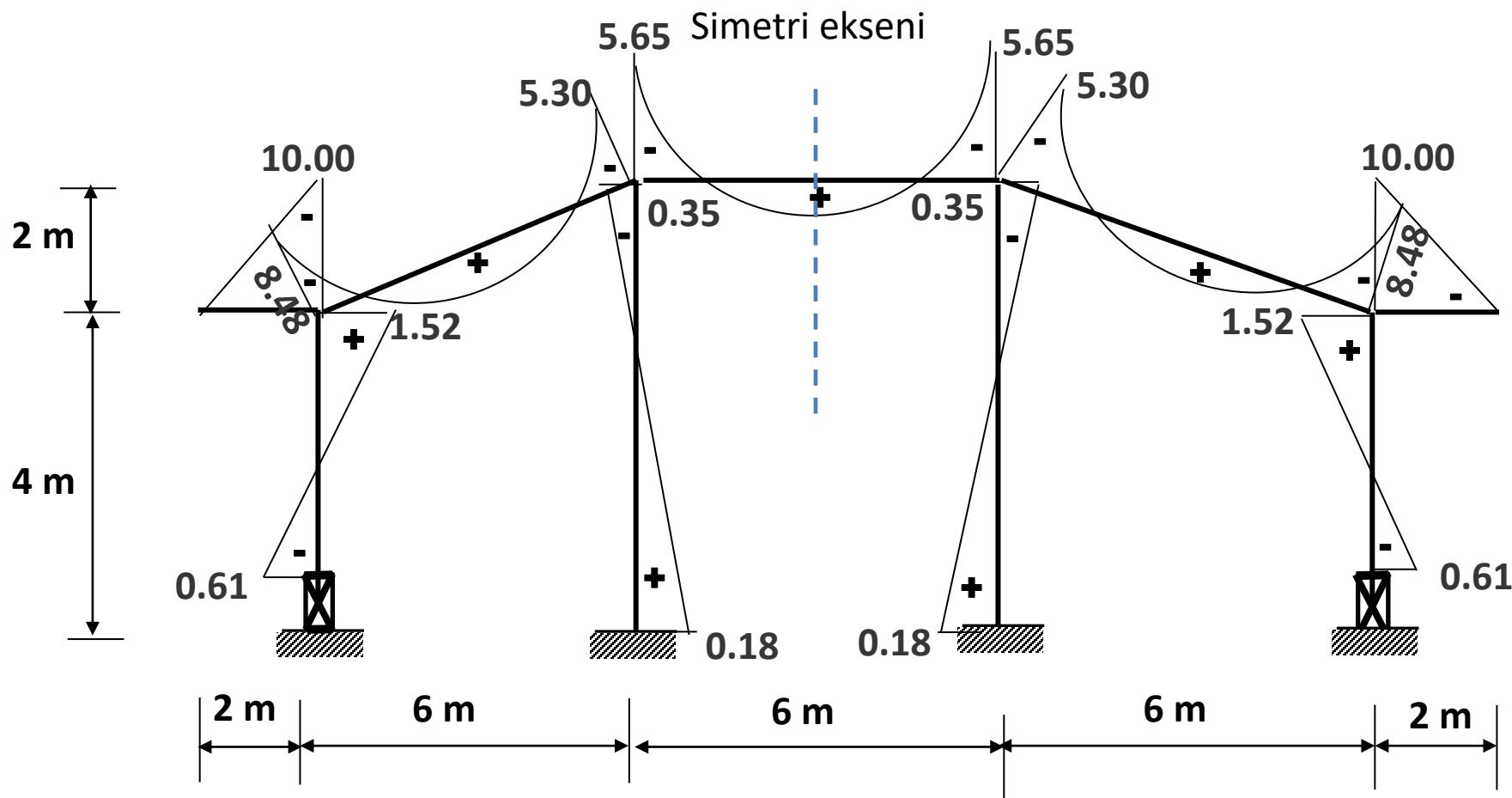
		(2-3)	(3-2)	(3-4)	(3-3')
		0.65	0.50	0.25	0.25
-10.00			-6.00	6.00	
1.40	6.00	1.30			
	2.60	-0.65	-0.33	-0.32	
0.12	-0.33	0.10			
	0.21	-0.05	-0.025	-0.025	
0.01	-0.02	-5.30	0.35	5.65	
1.52	0.01				
(1-2)	8.48				
	(1-1')				
0.20	0.80				
0.70					
-0.14	0.56				
0.06					
0.01	0.05				
0.63	-0.61				

Diagram showing a cross section with dimensions and forces. A horizontal double-headed arrow labeled $1/2$ spans the width of the cross-section. Three arrows point from the left towards the center of the cross-section.

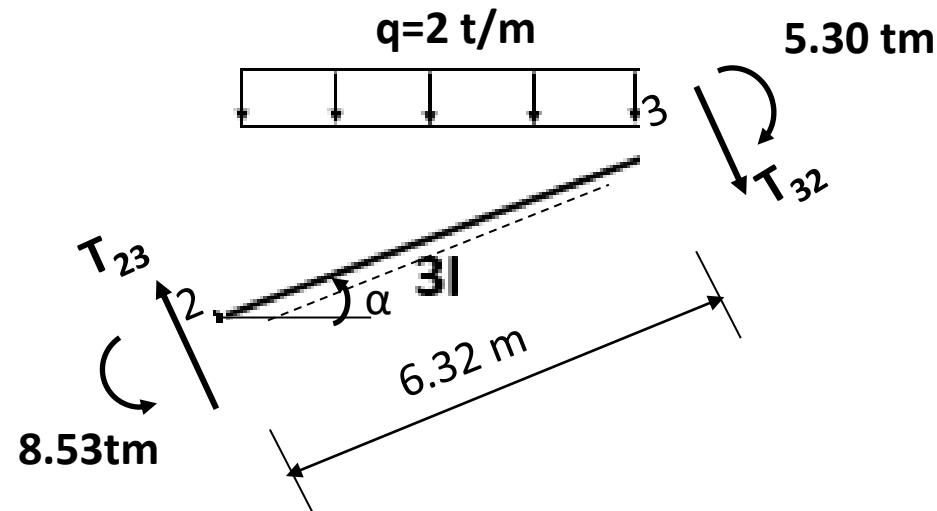
4. Dönüştürme



5. Moment diyagramı



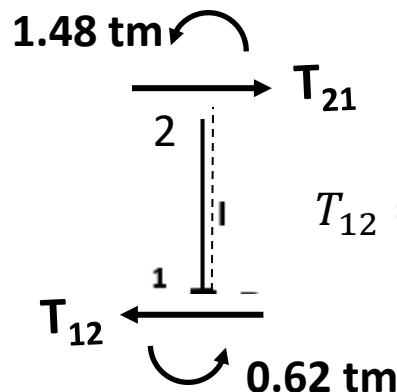
6. Kesme kuvvetlerinin hesabı



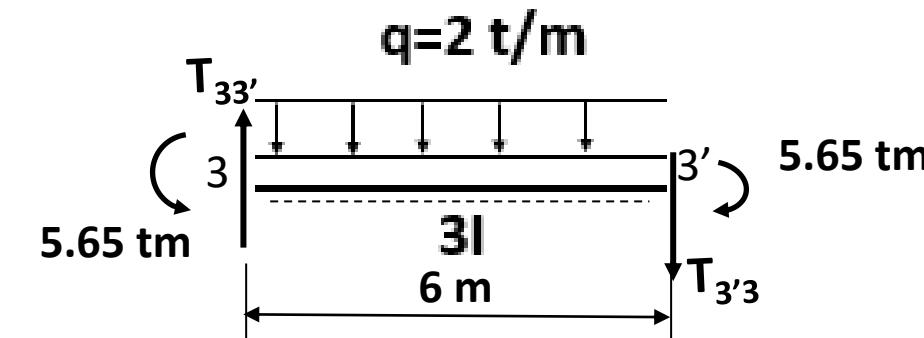
$$T_{konsol} = -5 \text{ t}$$

$$T_{23} = \frac{2 * 6}{2} \frac{6}{6.32} + \frac{8.53 - 5.30}{6.32} = 6.20 \text{ t}$$

$$T_{23} = -\frac{2 * 6}{2} \frac{6}{6.32} + \frac{8.53 - 5.30}{6.32} = -5.18 \text{ t}$$



$$T_{12} = T_{21} = \frac{0.62 + 1.48}{4} = 0.52 \text{ t}$$



$$T_{33'} = \frac{2 * 6}{2} + \frac{5.65 - 5.65}{6.0} = 6 \text{ t} = -T_{3'3}$$

6. Kesme kuvvetlerinin hesabı

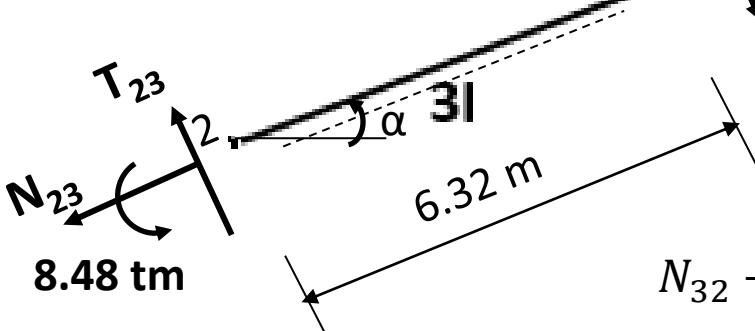
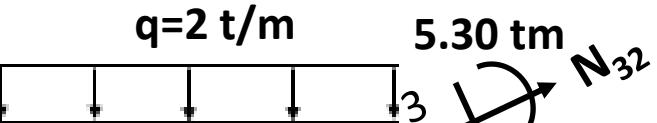
0.35 tm

T_{34}

$$T_{34} = T_{43} = \frac{-0.18 - 0.35}{6} = -0.08 t$$

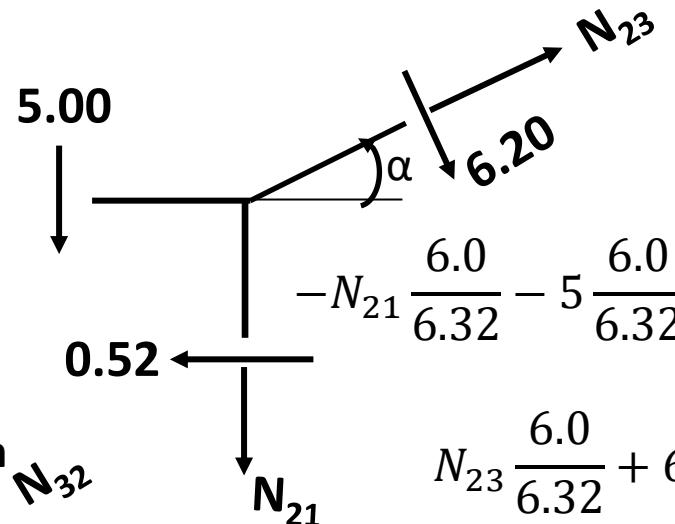
T_{43}

0.18 tm



7. Normal kuvvetlerinin hesabı

$$\sin\alpha = \frac{2}{6.32} \quad \cos\alpha = \frac{6}{6.32}$$

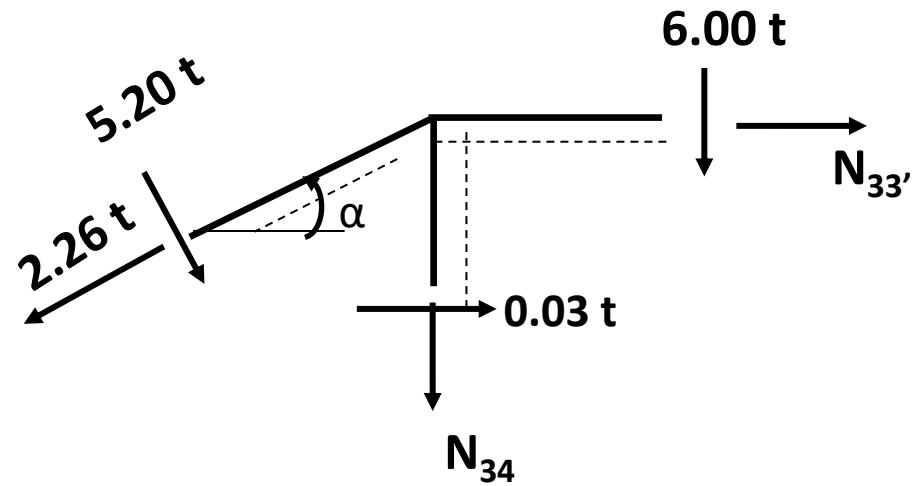


$$-N_{21} \frac{6.0}{6.32} - 5 \frac{6.0}{6.32} - 6.20 + 0.52 * \frac{2}{6.32} = 0 \quad N_{32} = -11.35 t$$

$$N_{23} \frac{6.0}{6.32} + 6.20 * \frac{2}{6.32} - 0.52 = 0 \quad N_{23} = -1.54 t$$

$$N_{32} - N_{23} - 2 * 6 * \frac{2}{6.32} = 0 \quad N_{32} = 2.26 t$$

7. Normal kuvvetlerinin hesabı



$$N_{33'} = 2.26 * \frac{6.00}{6.32} - 5.20 \frac{2.00}{6.32} - 0.03 = 0.43 \text{ t}$$

$$N_{33'} = 0.43 \text{ t}$$

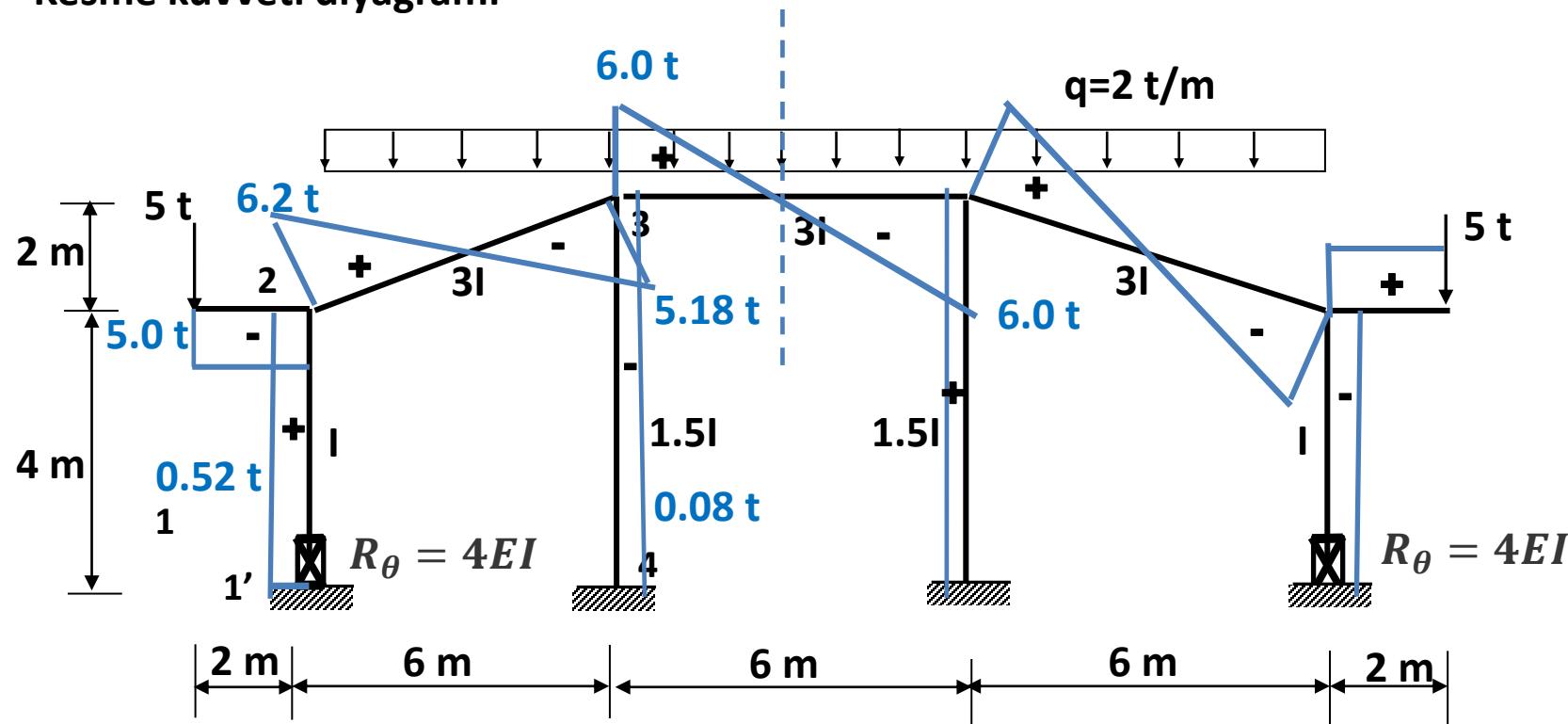
$$N_{34} = -6.00 - 5.20 * \frac{6.00}{6.32} - 2.26 \frac{2.00}{6.32} = -11.56 \text{ t}$$

$$\sin\alpha = \frac{2}{6.32} \quad \cos\alpha = \frac{6}{6.32}$$

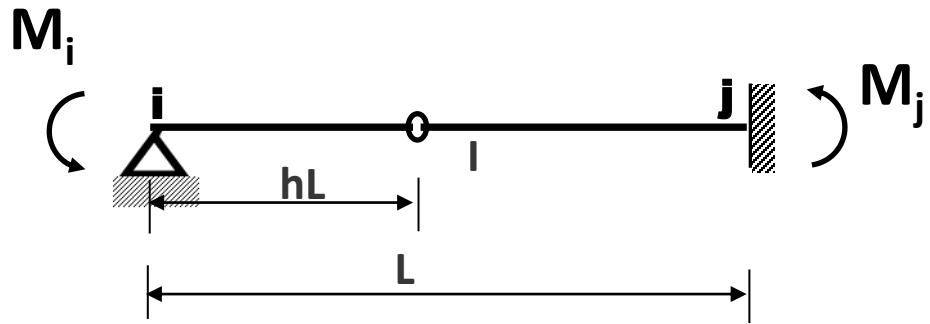
$$N_{34} = -11.56 \text{ t}$$

Simetri ekseni

6. Kesme kuvveti diyagramı



MAFSALLI SİSTEMLER



$$\theta_i = \frac{M_i}{3EI} \frac{3h^2 - 3h + 1}{h^2}$$

$$M_j = M_i \frac{1-h}{h}$$

$$\frac{M_j}{M_i} = \mu_{ij} = \frac{1-h}{h}$$

$$h = 1 \text{ için } \mu_{ij} = 0$$

$$h = \frac{2}{3} \text{ için } \mu_{ij} = \frac{1}{2} \quad h = 0.5 \text{ için } \mu_{ij} = 1$$

$$h = 0 \text{ için } \mu_{ij} = \infty$$

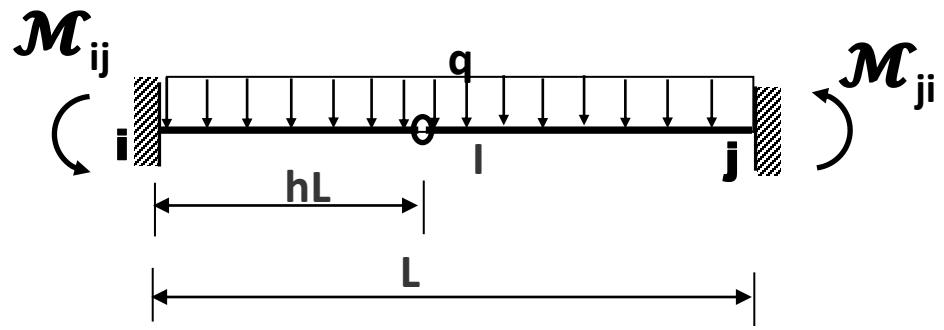
$$\theta_i = 1 \quad M_i = m_{i\theta_i}$$

$$m_{i\theta_i} = \frac{3EI}{L} \frac{h^2}{3h^2 - 3h + 1}$$

$$h = 1 \text{ ise } m_{i\theta_i} = m_{i\theta_i} = \frac{3EI}{L}$$

$h = \frac{2}{3}$ ise $m_{i\theta_i}$ maksimum olur.

$$m_{\theta_{i_{max}}} = \frac{4EI}{L}$$



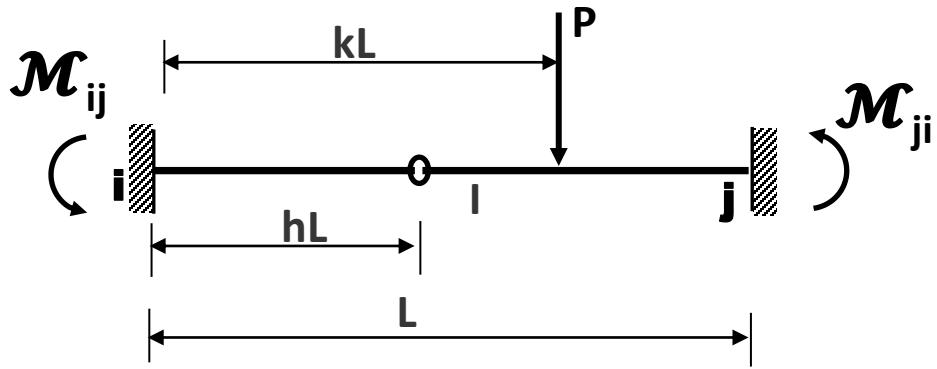
$$\mathcal{M}_{ij} = \frac{qL^2}{8} \frac{h(6h^2 - 8h + 3)}{3h^2 - 3h + 1}$$

$$\mathcal{M}_{ji} = -\frac{qL^2}{8} \frac{(1-h)(6h^2 - 8h + 3)}{3h^2 - 3h + 1}$$

özel hal $h = 0$ $\mathcal{M}_{ij} = 0$ $\mathcal{M}_{ji} = \frac{qL^2}{8}$

$$h = 1 \quad \mathcal{M}_{ij} = \frac{qL^2}{8} \quad \mathcal{M}_{ji} = 0$$

$$h = 0.5 \quad \mathcal{M}_{ij} = -\mathcal{M}_{ji} = \frac{qL^2}{8}$$



$$M_{ij} = PL \left[k - \frac{k^2 h (3h - k)}{2(3h^2 - 3h + 1)} \right] \quad k \leq h$$

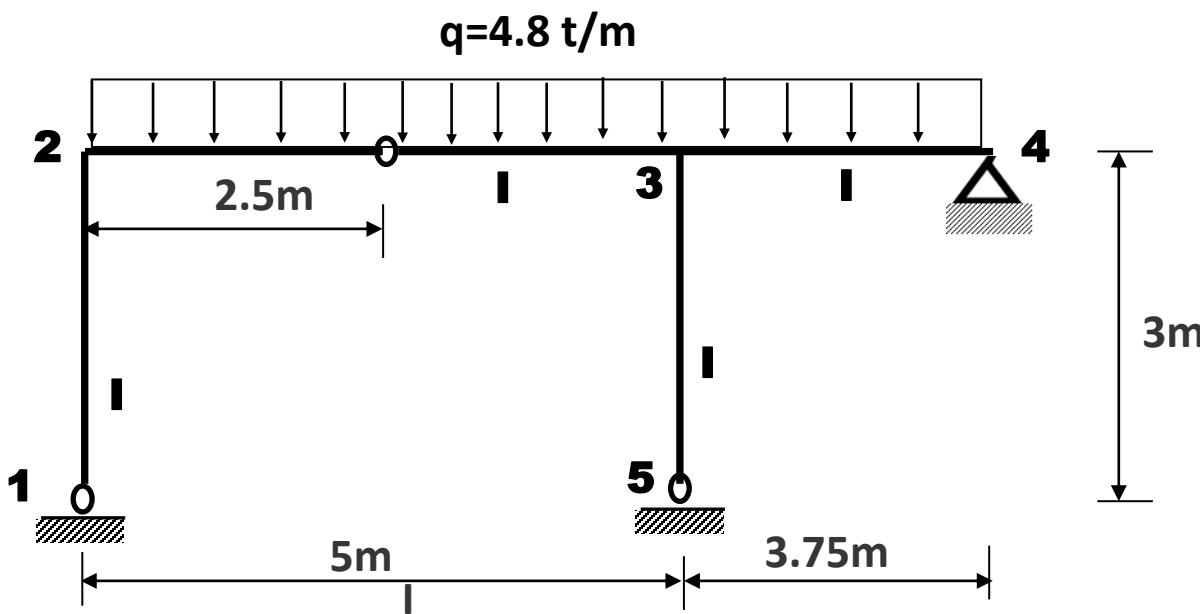
$$M_{ji} = -PL \left[\frac{k^2 (1 - h) (3h - k)}{2(3h^2 - 3h + 1)} \right] \quad k \leq h$$

$$M_{ij} = PL \left[\frac{h(1 - k)^2 (k + 2 - 3h)}{2(3h^2 - 3h + 1)} \right] \quad k \geq h$$

$$M_{ji} = -PL \left[1 - k - \frac{(1 - k)^2 (1 - h) (k + 2 - 3h)}{2(3h^2 - 3h + 1)} \right] \quad k \geq h$$

$$k = h \text{ is } e \quad M_{ij} = PL \frac{h(1 - h)^3}{3h^2 - 3h + 1} \quad M_{ji} = -PL \frac{h^3(1 - h)}{3h^2 - 3h + 1}$$

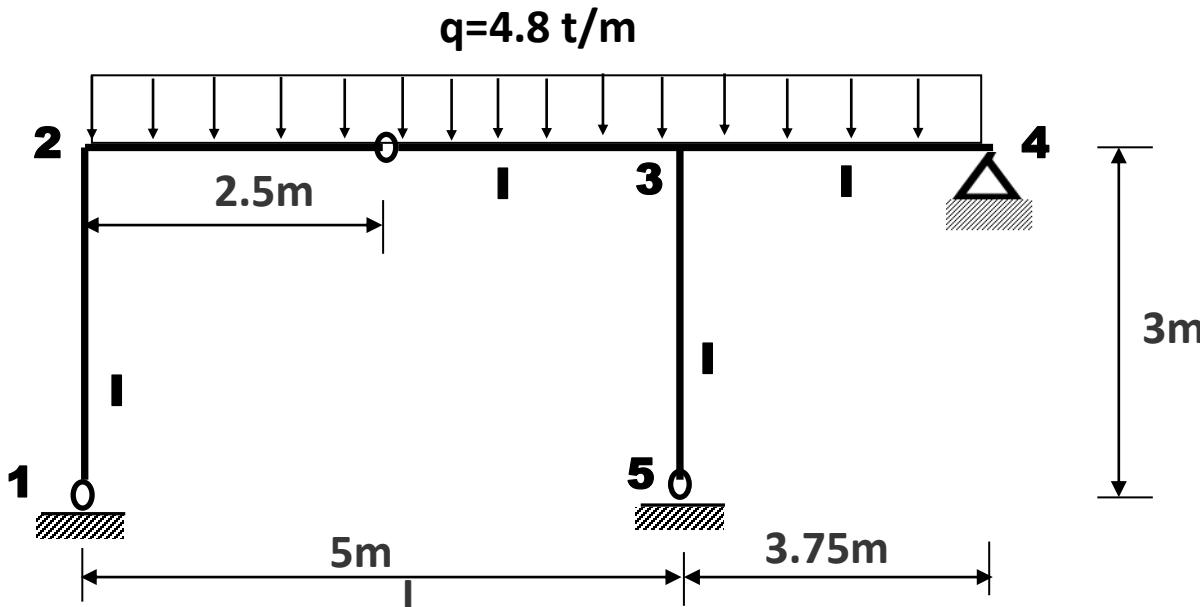
UYGULAMA 4



1. Ankastrelik momentleri:

$$\mathcal{M}_{23} = -\mathcal{M}_{32} = \frac{4.8 * 5^2}{8} = 15 \text{ tm} \quad \mathcal{M}_{34} = \frac{4.8 * 3.75^2}{8} = 8.44 \text{ tm}$$

UYGULAMA



2. Dağıtma sayıları:

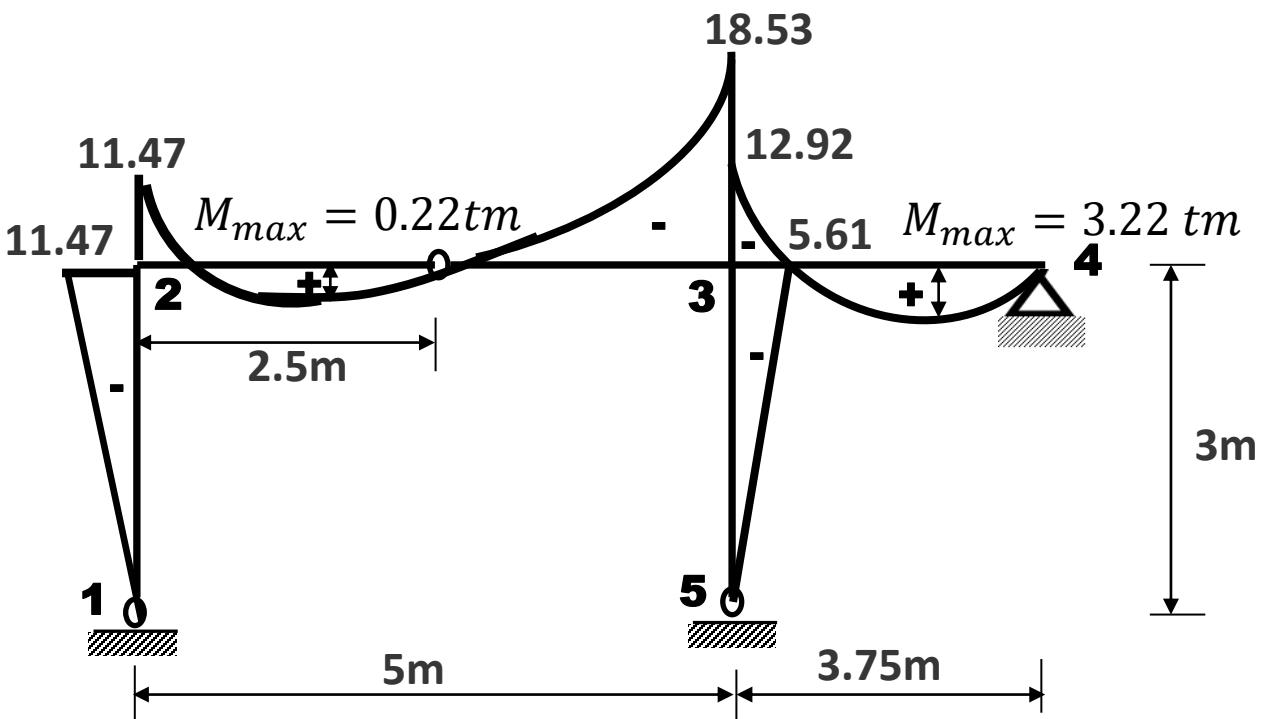
$$r_{21} = \frac{\frac{3EI}{3}}{\frac{3EI}{3} + \frac{3EI}{5}} = 0.625 \quad r_{23} = \frac{\frac{3EI}{5}}{\frac{3EI}{3} + \frac{3EI}{5}} = 0.375$$

$$r_{32} = \frac{\frac{3EI}{5}}{\frac{3EI}{5} + \frac{3EI}{3} + \frac{3EI}{3.75}} = 0.25 \quad r_{35} = \frac{\frac{3EI}{3}}{\frac{3EI}{5} + \frac{3EI}{3} + \frac{3EI}{3.75}} = 0.417 \quad r_{35} = \frac{\frac{3EI}{3.75}}{\frac{3EI}{5} + \frac{3EI}{3} + \frac{3EI}{3.75}} = 0.333$$

3. Cross dengelemesi:

(2-1)		(2-3)				
1	0					
0.625	0.375	0.250	0.417	0.333		
-9.38	15.00	-15.00		8.44		
-1.90	3.04	3.04	5.08	4.06		
-0.18	-1.14	-1.14				
0.29	0.29	0.29	0.48	0.38		
-0.11	-0.11	-0.11				
0.03	0.03	0.03	0.05	0.04		
-0.01	-0.01	-0.01				
-11.48	-11.47	-18.53	5.61	12.92		

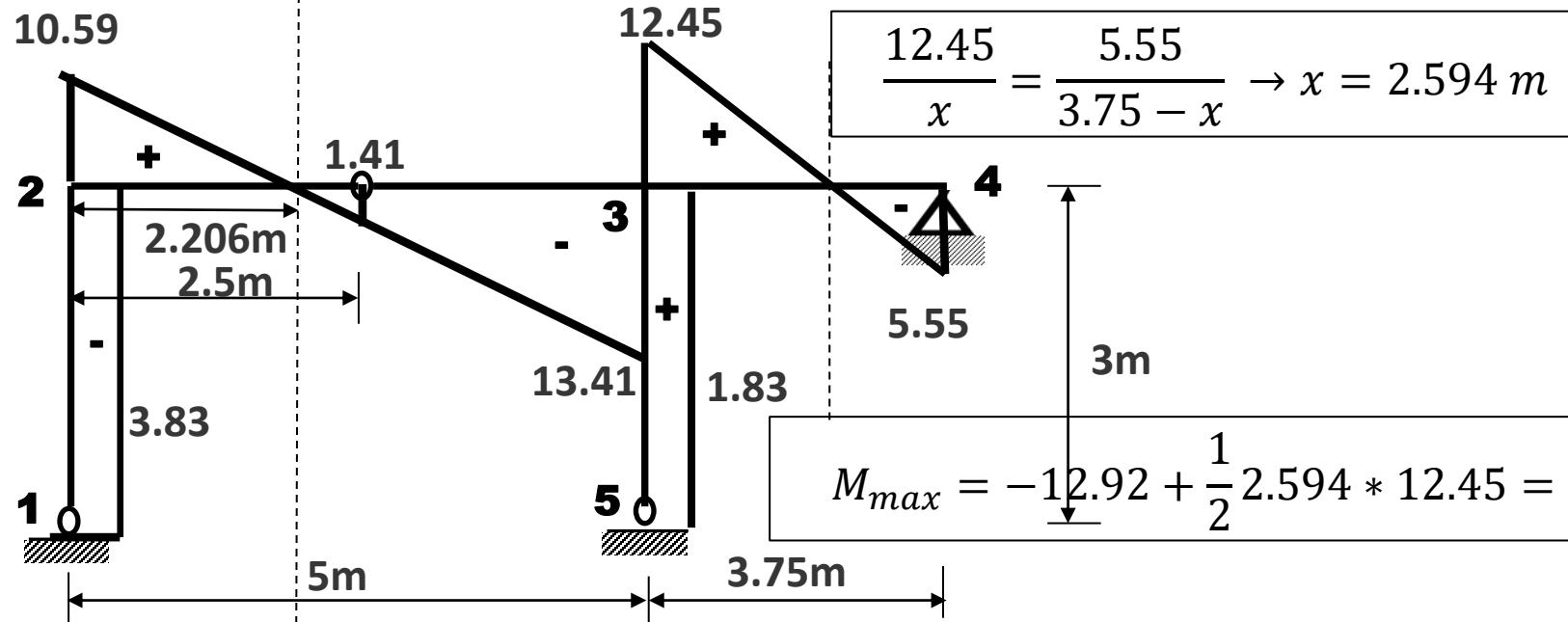
4. Moment diyagramı:



5. Kesme kuvveti diyagramı:

$$\frac{10.59}{x} = \frac{13.41}{5-x} \rightarrow x = 2.206$$

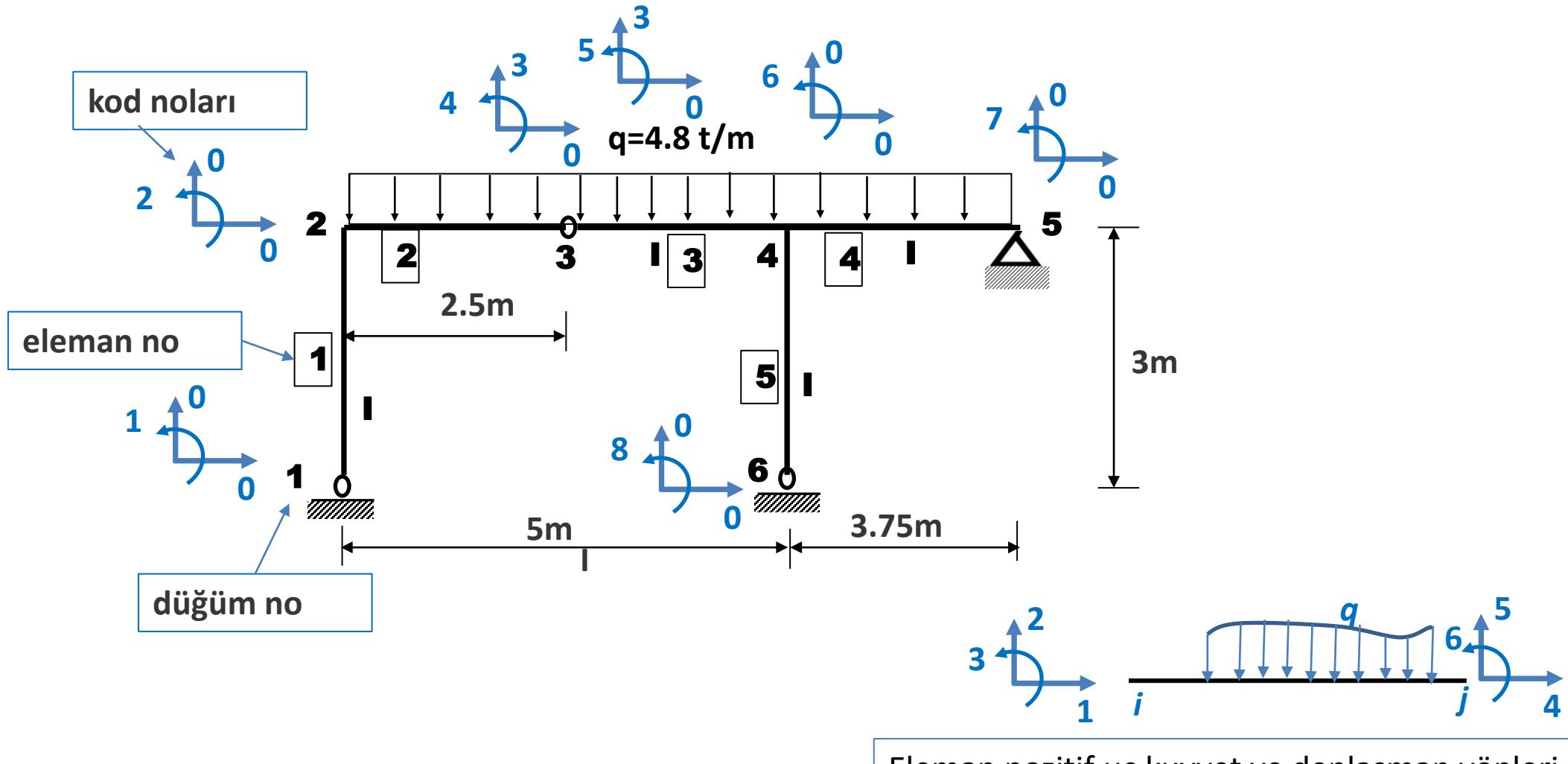
$$\frac{12.45}{x} = \frac{5.55}{3.75-x} \rightarrow x = 2.594 \text{ m}$$



$$M_{max} = -11.47 + \frac{1}{2} 2.206 * 10.59 = 0.22 \text{ tm}$$

5.61

RİJİTLİK MATRİSİ YÖNTEMİ İLE ÇÖZÜM (SDB88 PROGRAM*)



Eleman pozitif uç kuvvet ve deplasman yönleri

RİJİTLİK MATRİSİ YÖNTEMİ İLE ÇÖZÜM (SDB88 PROGRAM*)

6) DÜZLEMİ İÇERİSİNDE YUKLU GENEL CERCEVELERİN STATİK HESABI :

MAFSALLI CERCEVE

ELEMAN SAYISI ----- = 5

DEPLASMAN SAYISI ----- = 8

DUGUM SAYISI ----- = 6

ELASTISITE MODULU ----- = 1

YUKLEME SAYISI ----- = 1

KAYMA DEFORMASYONLARI İHMAL EDİLİYOR

DUGUM	X	Y
1	0.00	0.00
2	0.00	3.00
3	2.50	3.00
4	5.00	3.00
5	8.75	3.00
6	5.00	0.00

ELEMAN	i	j	BOYU	ALAN	ATALET	K O D	N U M A R A L A R I
1	1	2	3.00	1.000	1.0000	0 0 1 0 0 2	
2	2	3	2.50	1.000	1.0000	0 0 2 0 0 4	
3	3	4	2.50	1.000	1.0000	0 3 5 0 0 6	
4	4	5	3.75	1.000	1.0000	0 0 6 0 0 7	
5	4	6	3.00	1.000	1.0000	0 0 6 0 0 8	

YUKLEME NO = 1

MAFSALLI CERCEVE

ANKASTRELIK UC KUVVETLERİ

ELEMAN	Ni	Ti	Mi	Nj	Tj	Mj
1	0.000	0.000	0.000	0.000	0.000	0.000
2	0.000	-6.000	-2.500	0.000	-6.000	2.500
3	0.000	-6.000	-2.500	0.000	-6.000	2.500
4	0.000	-9.000	-5.625	0.000	-9.000	5.625
5	0.000	0.000	0.000	0.000	0.000	0.000

UC KUVVETLERİ

ELEMAN	Mij	Mji	Tij	Tji	Nj	ACIKLIK M.
1	0.00	-11.48	-3.83	3.83	0.00	
2	11.48	-0.00	10.59	1.41	0.00	0.21
3	-0.00	-18.52	-1.41	13.41	0.00	
4	12.92	0.00	12.45	5.55	0.00	3.21
5	5.60	-0.00	1.87	-1.87	0.00	